

Through the hidden veins of the earth: *How do water and solutes get to Silver Springs?*

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Michael D. Annable², Kirk Hatfield²

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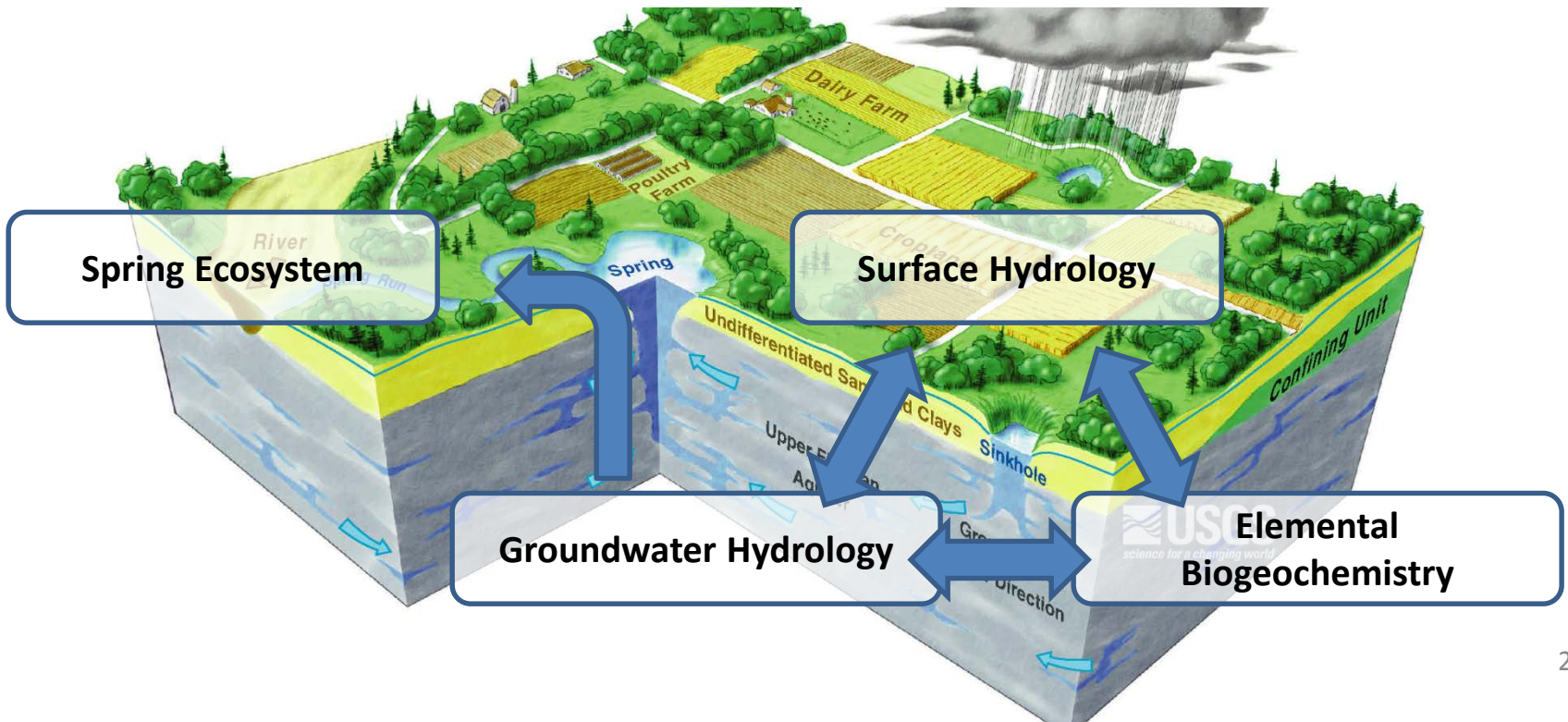
² Engineering School of Sustainable Infrastructure & Environment, University of Florida



Collaborative Research Initiative on Sustainability and Protection of Springs [CRISPS]

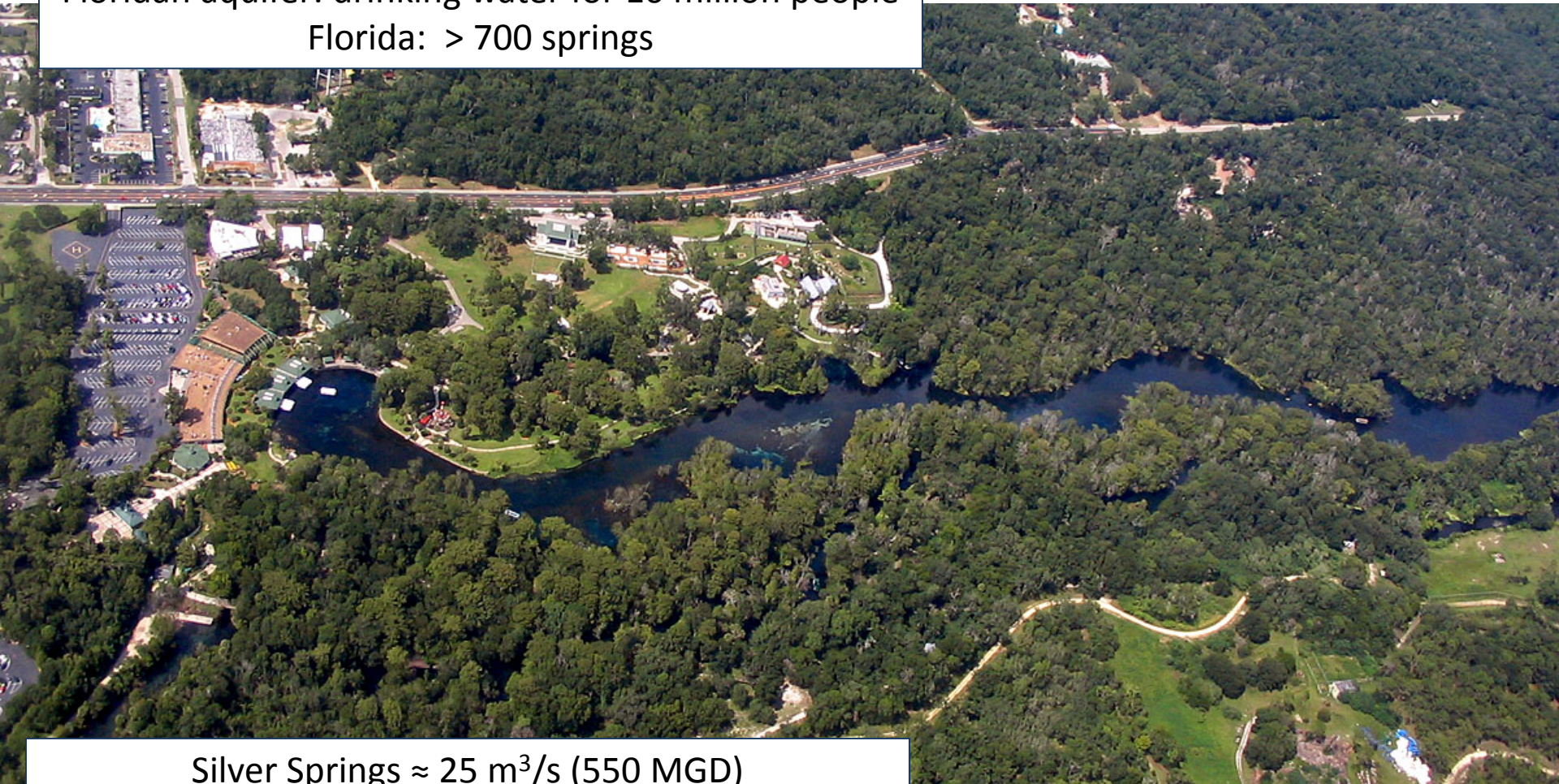


UF: Mike Annable, Matt Cohen, Tom Frazer, Wendy Graham, Patrick Inglett, Jim Jawitz, David Kaplan, Jon Martin, Todd Osborne, K. Ramesh Reddy



Silver Springs: First magnitude discharge

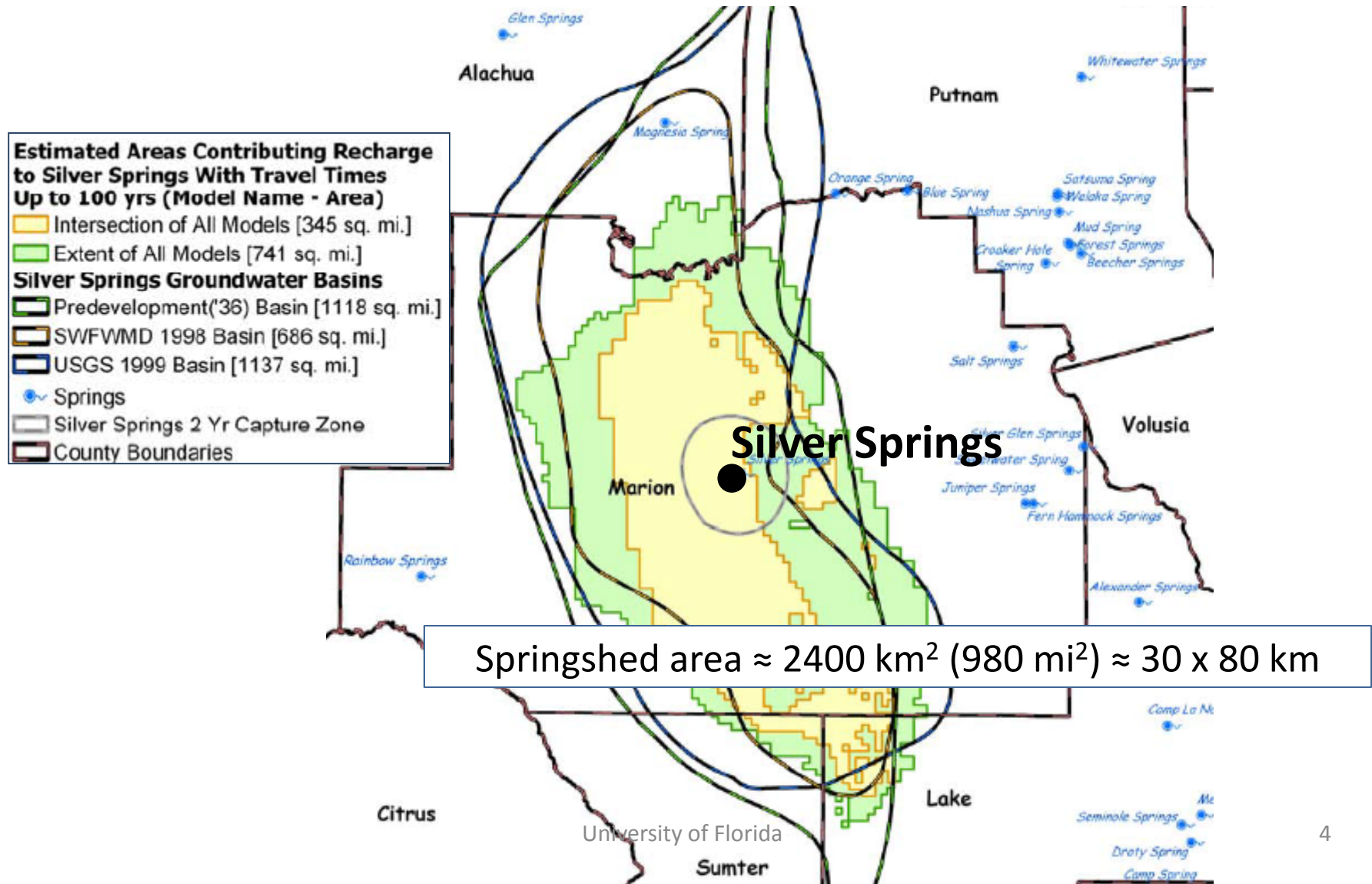
Floridan aquifer: drinking water for 10 million people
Florida: > 700 springs



Silver Springs $\approx 25 \text{ m}^3/\text{s}$ (550 MGD)
“First magnitude” $> 2.8 \text{ m}^3/\text{s}$ (USA ~ 75 , Florida ~ 25)

Springshed size + geometry

based on heads vs numerical porous media models

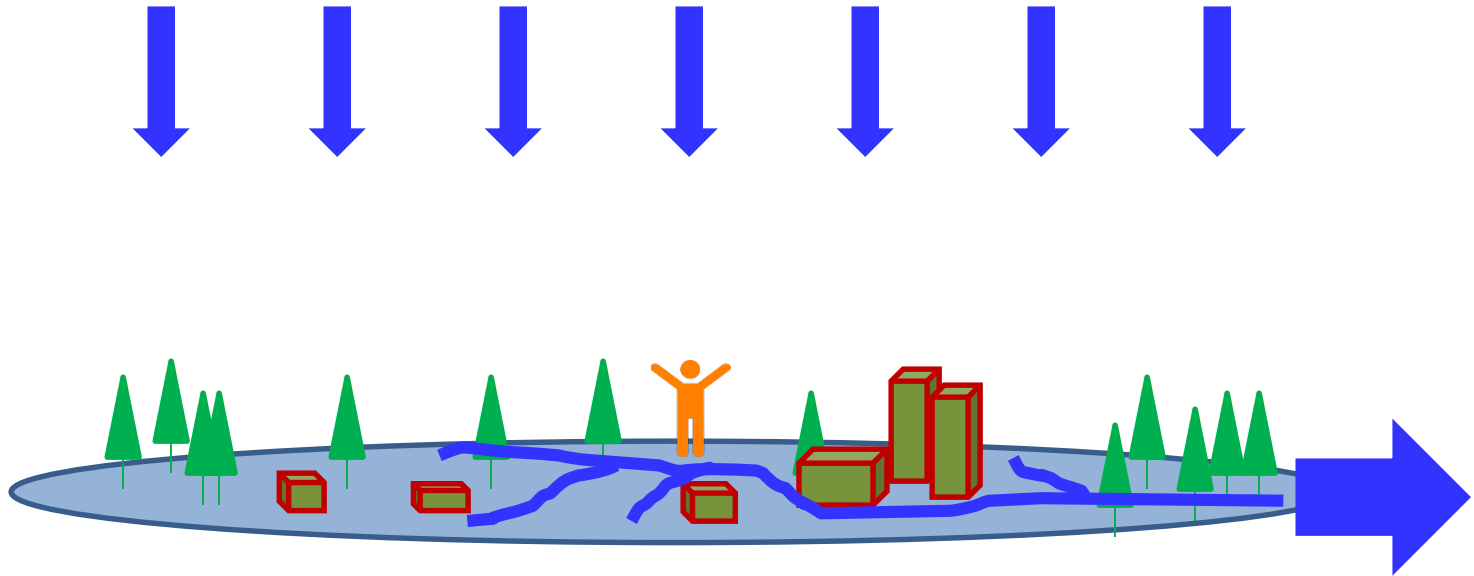


problem description

over several decades, discharge has been declining and
nitrate concentrations rising

why? where? how?

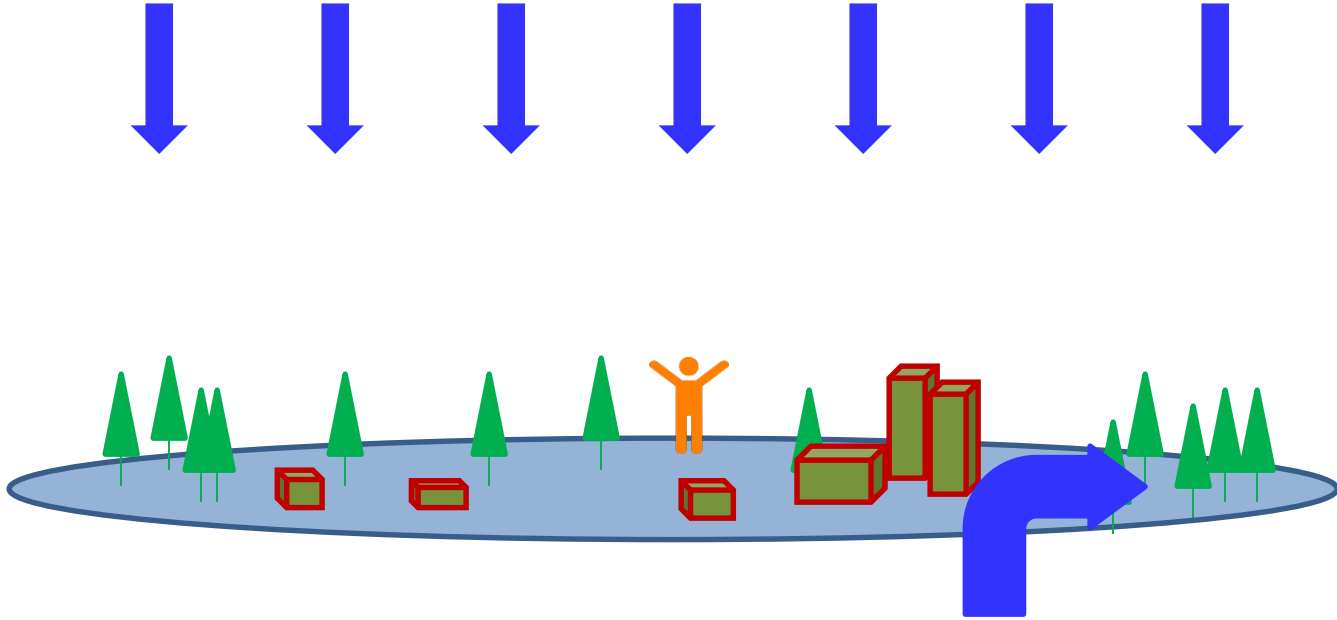
parsimonious models to assist resource managers

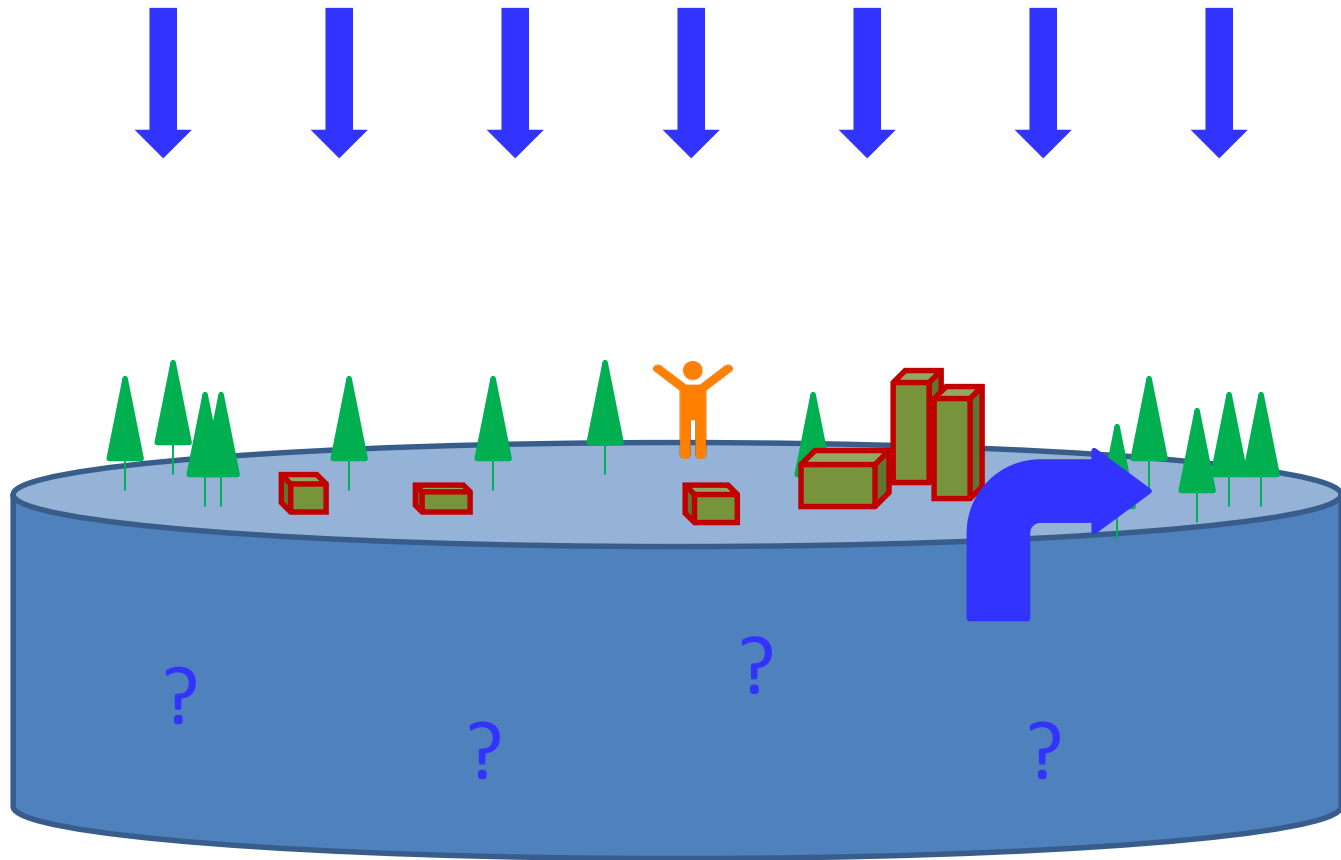


A watershed

“that area of land, a bounded hydrologic system, within which all living things are inextricably linked by their common water course and where, as humans settled, simple logic demanded that they become part of a community.”

John Wesley Powell, 1890

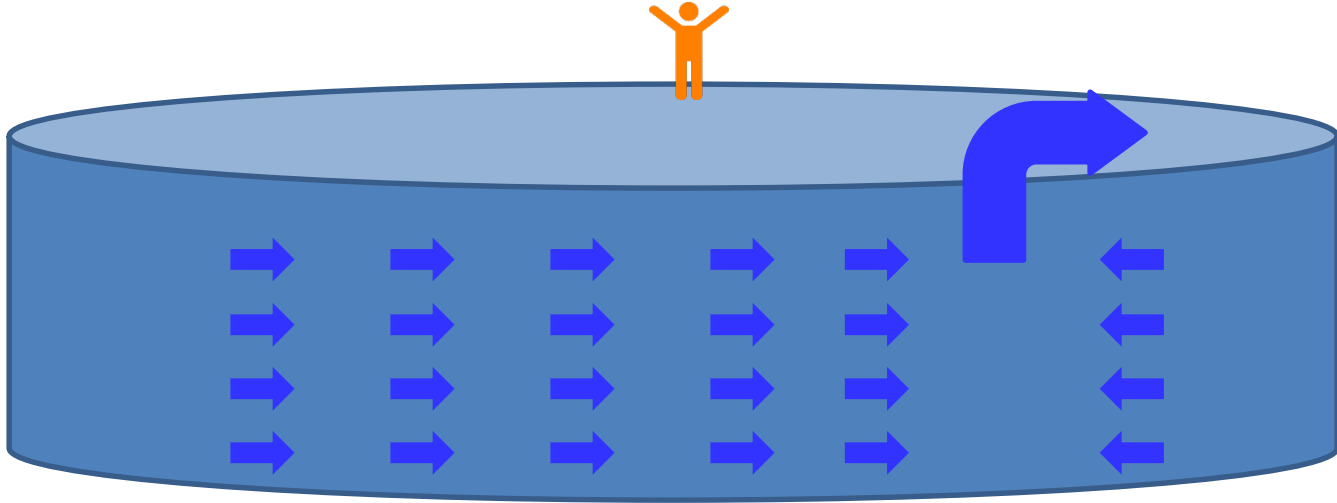


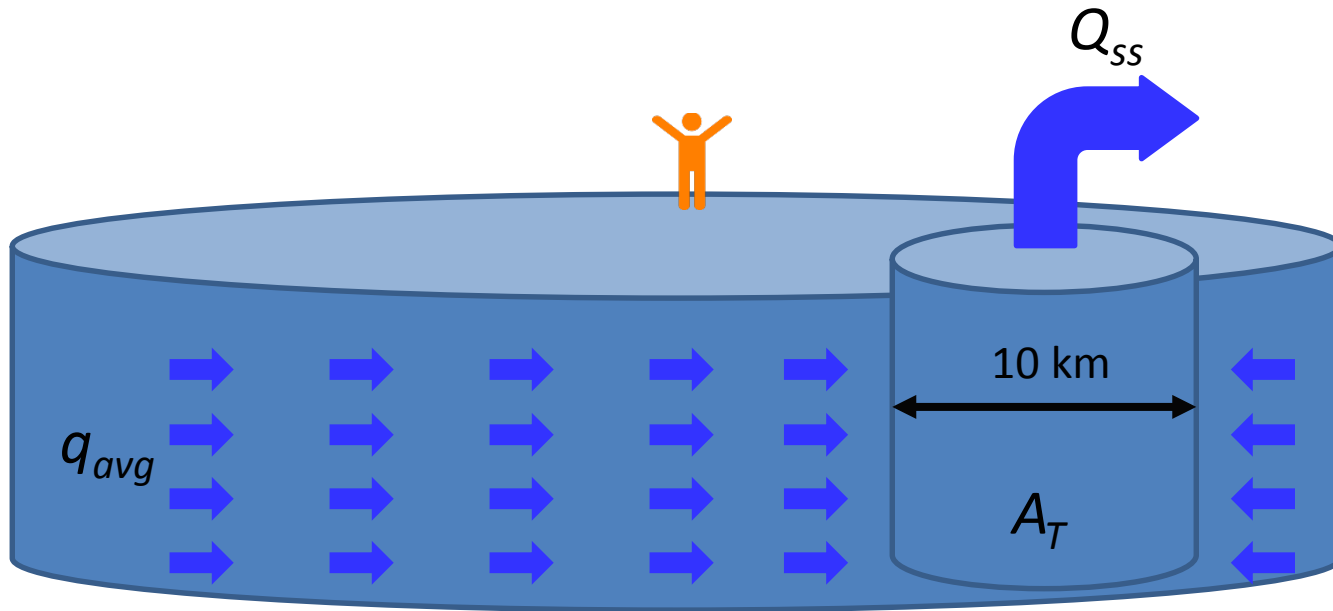


“In the case of a well sunk by a proprietor in his own land, the water which feeds it from a neighboring soil does not flow openly in the sight of the neighboring proprietor, but through the *hidden veins of the earth beneath its surface; no man can tell what changes these underground sources have undergone in the progress of time.*”

Acton v. Blundell

Texas case based on principles of English common law, 1843





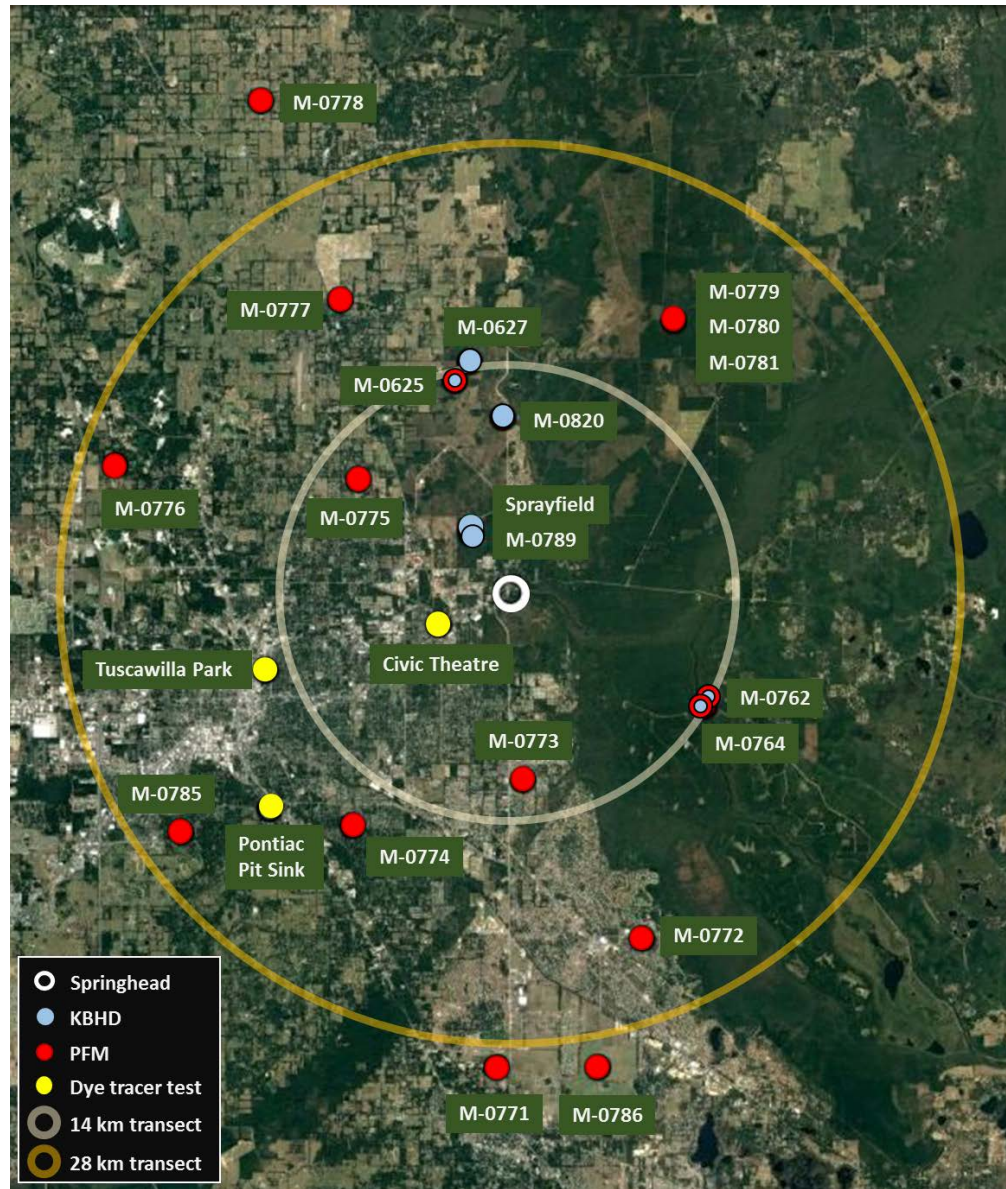
$$Q_{ss} = q_{avg} A_T$$

$$A_T = (\pi d)h$$

$$\underline{\underline{q_{avg} = A_T / Q_{ss}}}$$

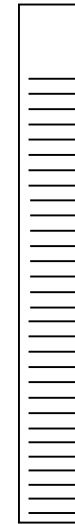
	10-km traverse	20-km traverse
Spring flow	20 m ³ /s	20 m ³ /s
Depth	50 m	50 m
Perimeter	31 km	63 km
q_{avg}	1.1 m/d	0.55 m/d

Method	PFM (16 wells)	KBHD (7 wells)	DTT (3 sites) Introduction location
	M-0625 (3)	M-0625 (2)	Civic Theatre Drainage Retention Area (8)
	M-0762 (3)	M-0627 (1)	Tusawilla Park Stormwater Drainage well (1)
	M-0764 (3)	M-0762 (2)	Pontiac Pit Sink (3)
	M-0771 (3)	M-0764 (1)	
	M-0772 (3)	M-0789 (6)	
	M-0773 (3)	M-0820 (4)	
	M-0774 (3)	Sprayfield (5)	
	M-0775 (3)		
	M-0776 (3)		
	M-0777 (3)		
	M-0778 (3)		
	M-0780 (3)		
	M-0781 (3)		
	M-0785 (3)		
	M-0786 (3)		
	M-0787 (3)		
Total	48	21	12

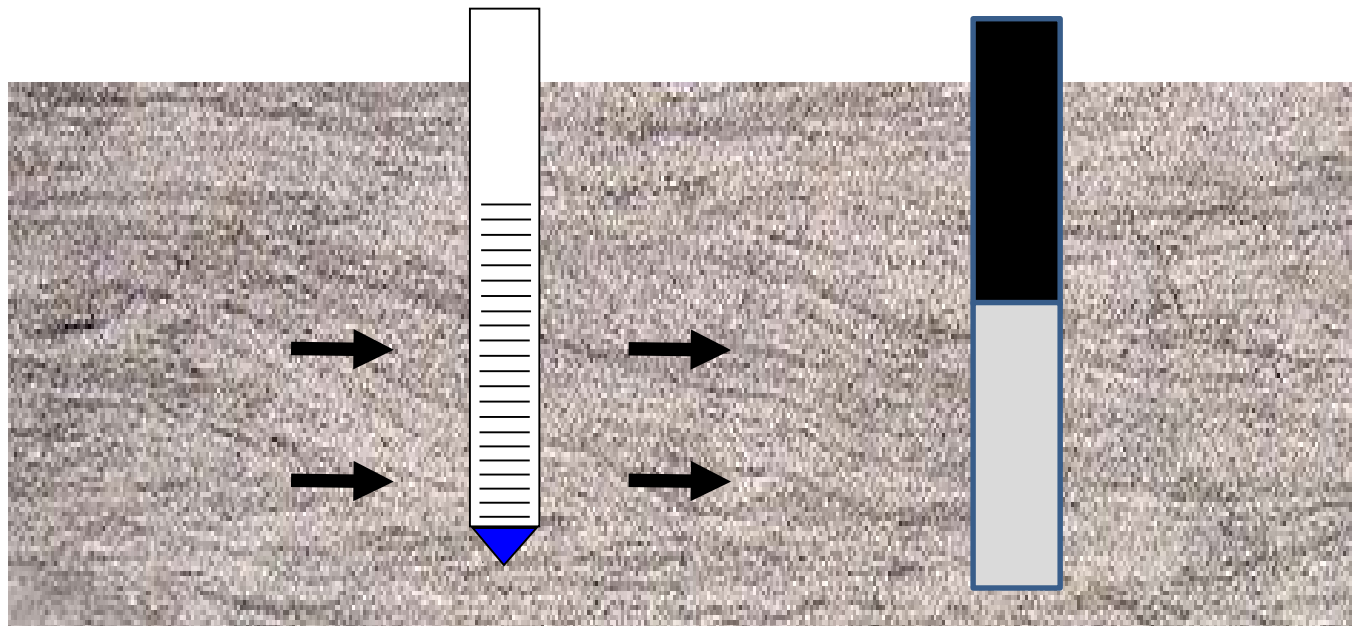


Passive Flux Meters

Granular Activated Carbon (GAC) contained in a permeable mesh inserted into the well screen

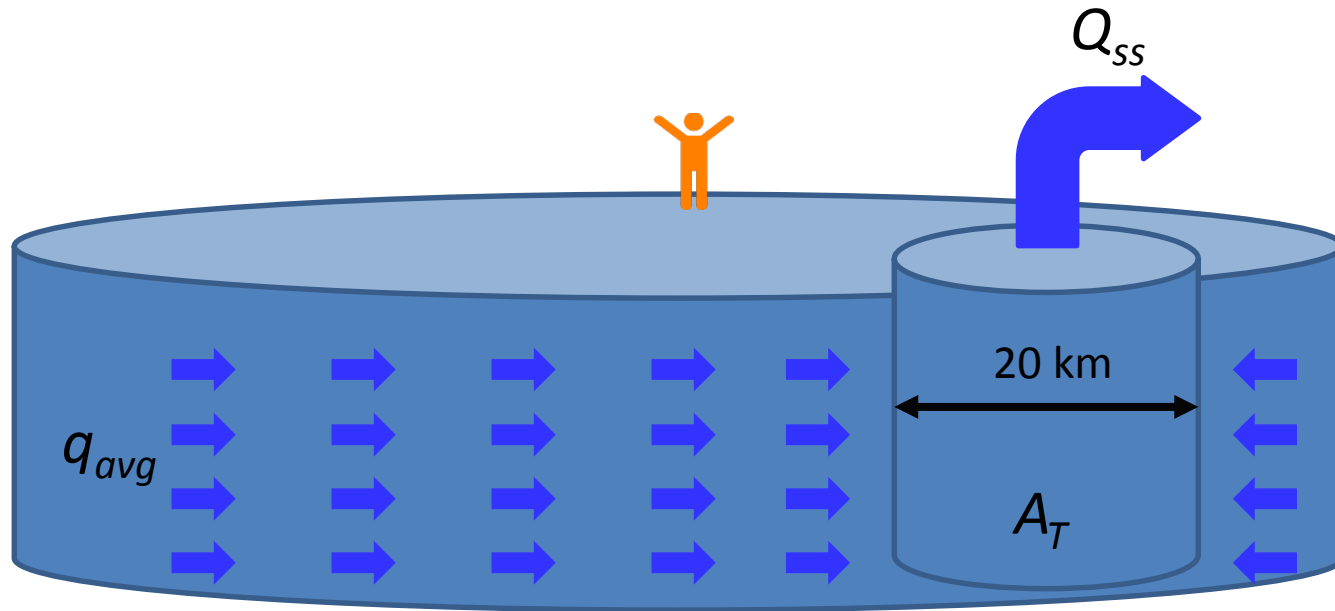


Modified PFM for open rock borehole applications in deeper wells









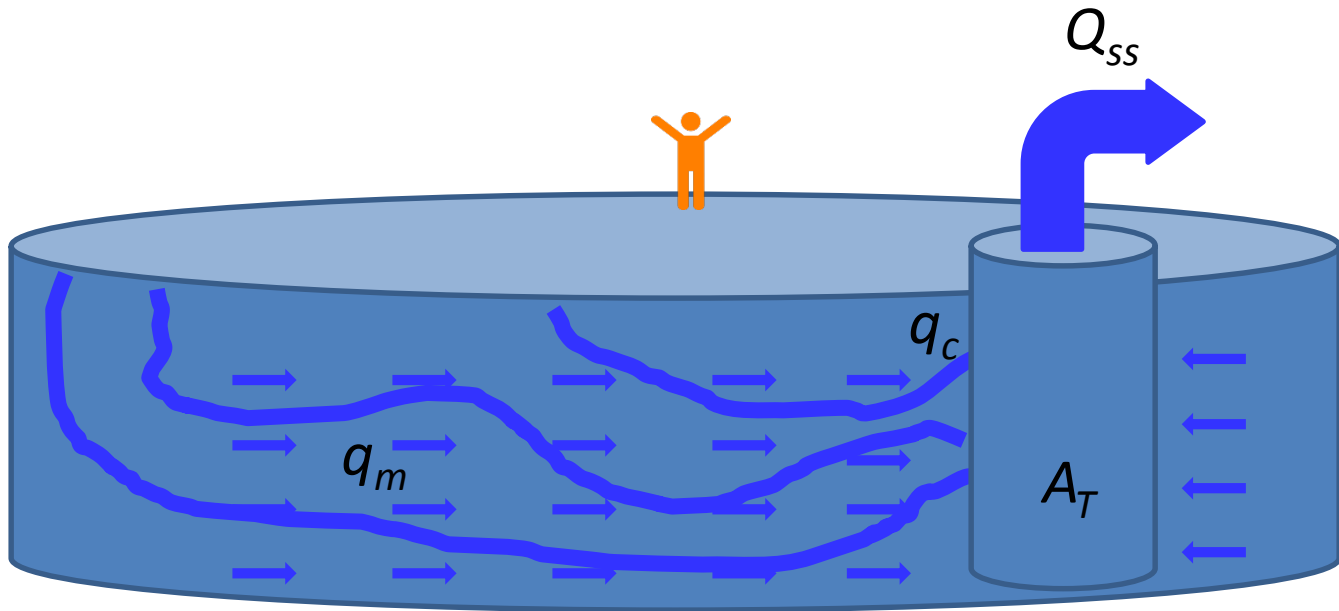
$$Q_{ss} = q_{avg} A_T$$

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$$q_{avg} = A_T / Q_{ss}$$

	10-km transect	20-km transect
Spring flow	20 m ³ /s	20 m ³ /s
Depth	50 m	50 m
Perimeter	31 km	63 km
q_{avg}	1.1 m/d	0.55 m/d

PFMs (n=16 wells)
0.06 ± 0.02 m/d



$$Q_{ss} = q_{avg} A_T$$

$$Q_{ss} = Q_m + Q_c$$

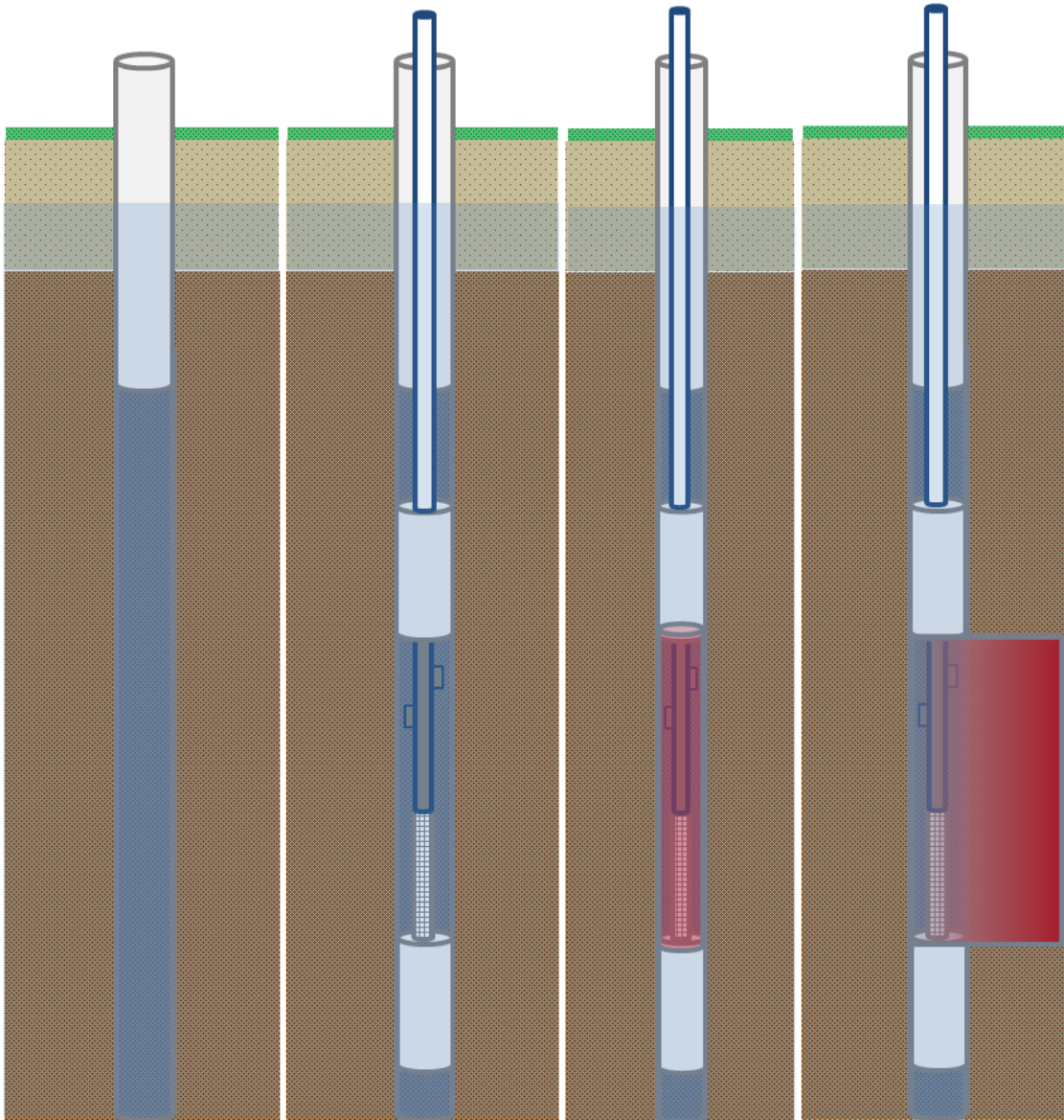
$$Q_{ss} = q_m A_m + q_c A_c$$

$$A_T = A_m + A_c$$

$$\underline{\underline{A_c/A_T = (q_{avg} - q_m)/(q_c - q_m)}}$$

	10-km transect	20-km transect
q_{avg}	1.1 m/d	0.55 m/d
q_m	??	??
q_c	??	??
A_c/A_T		
Q_c/Q_{ss}		

Borehole dilution concept

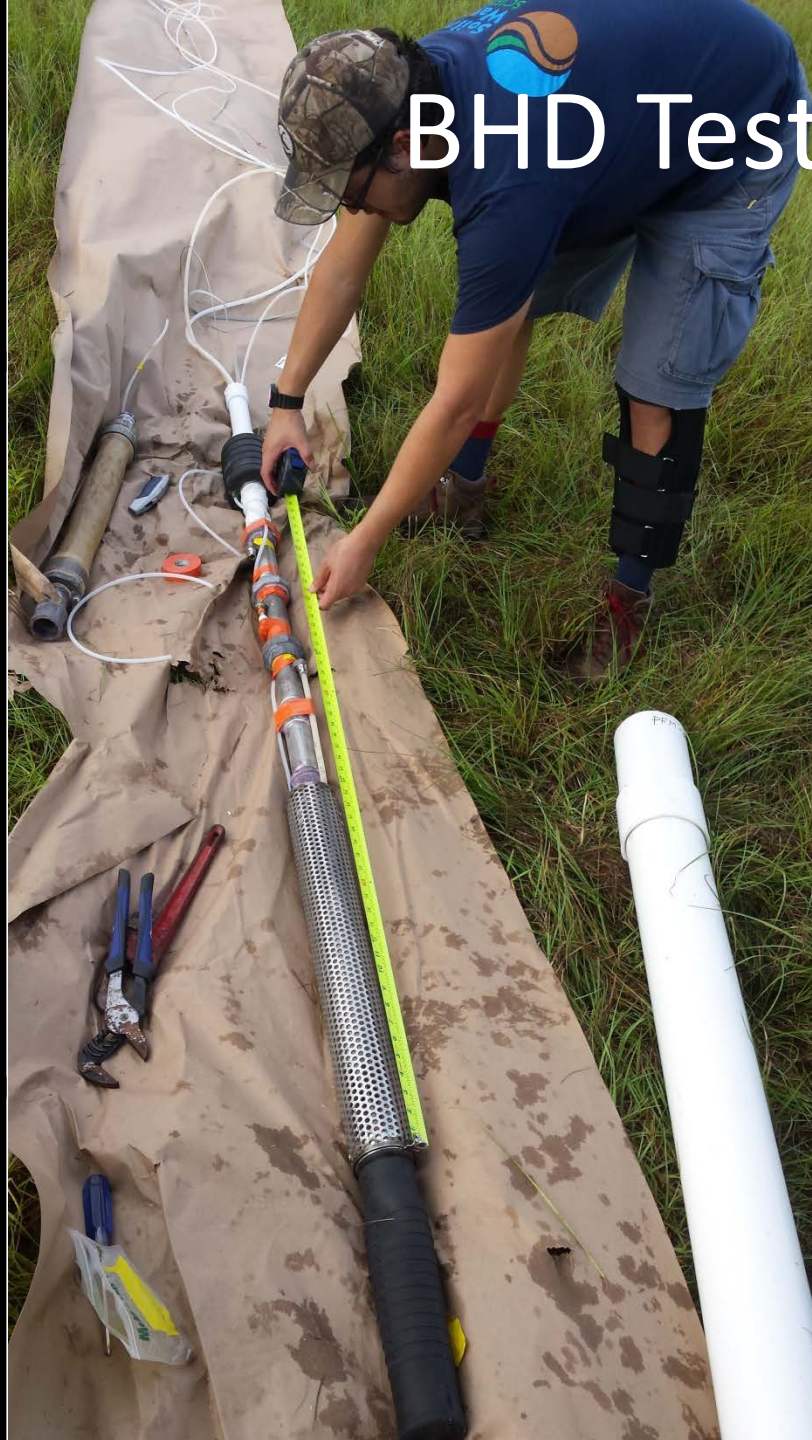


BHD test measures the rate at which a **pulse** of tracer is **diluted** in an **isolated** section of the borehole.

Dilution is attributed to horizontal water velocity

BHD Test Procedure

- Identify areas of interest
- Assemble KBHD device
- Deploy to target depth



M0789 - 122 ft



<https://www.youtube.com/watch?v=eQlfhUgzJ7g>

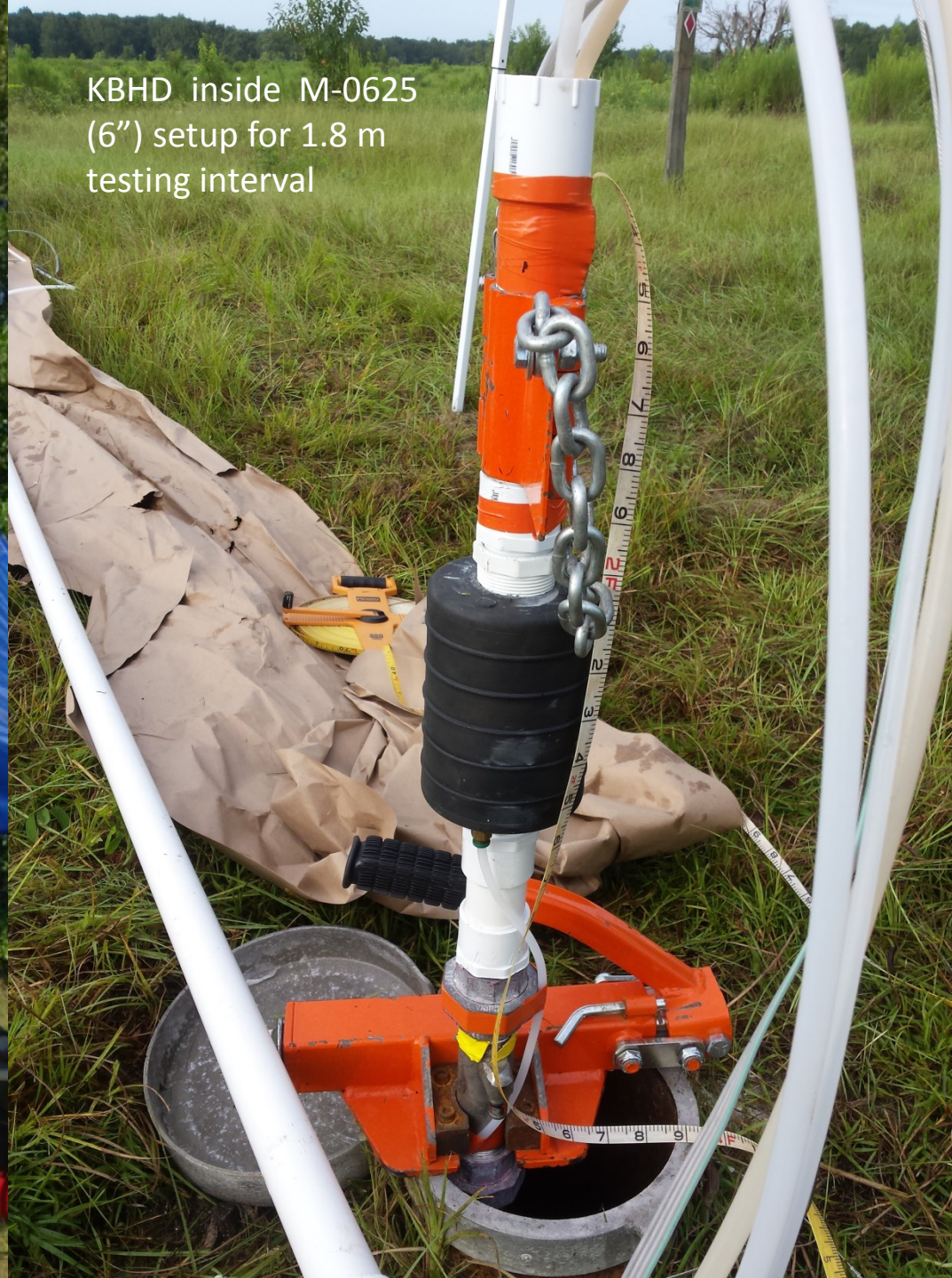
M0625



KBHD ready for deployment in well M-789 (4" setup for 3 m testing interval)



KBHD inside M-0625 (6" setup for 1.8 m testing interval)





KBHD inside M-0625
placement at 111-117 ft



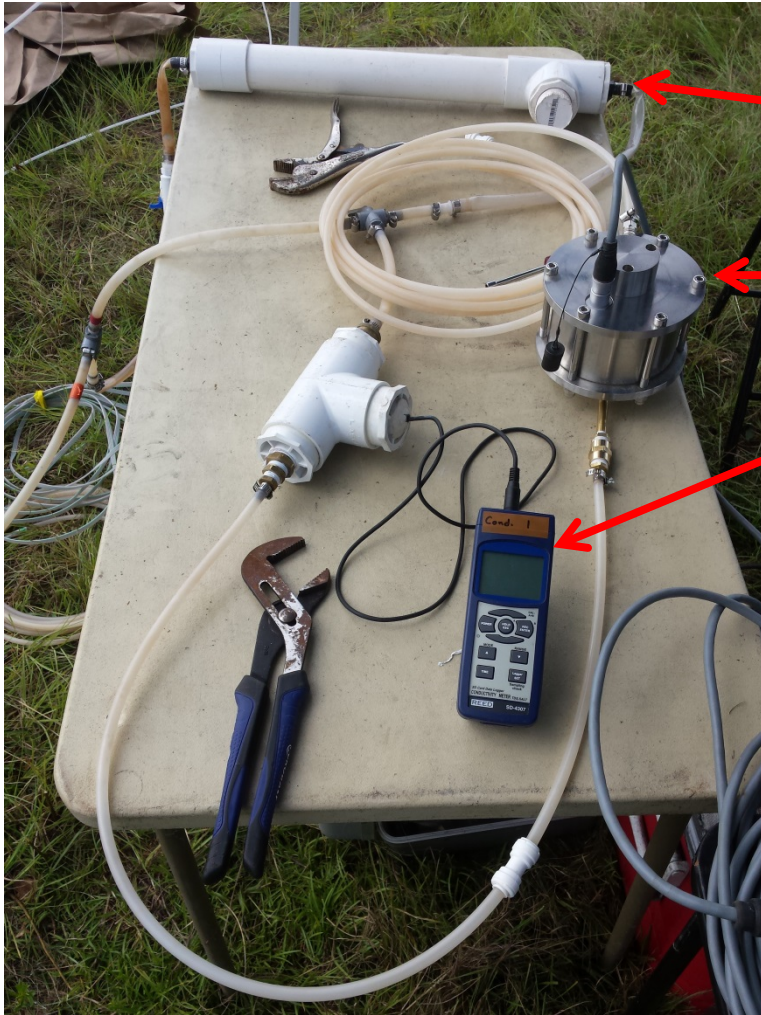
KBHD inside Sprayfield
well (4"), deployed in
83-88 ft. interval

BHD Test Procedure



- Purge well
- Inflate packers
- Release KCl + Rhodamine pulse
- Start recirculation
- Monitor electrical conductivity and fluorescence
- Purge well back to background conductivity levels

BHD Test Procedure



Pulse reservoir (KCl + Rhodamine solution)

Flourometer

Conductivity meter



214



OVERLOCK STITCHES

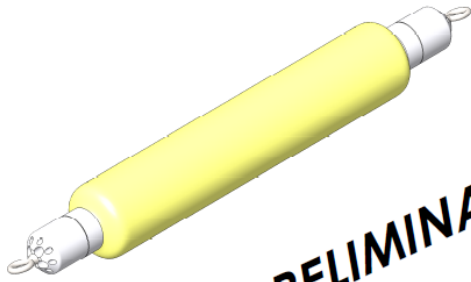
PIPET BULBS
MAGNETIC STIRRER

SYRINGES
FILTERS

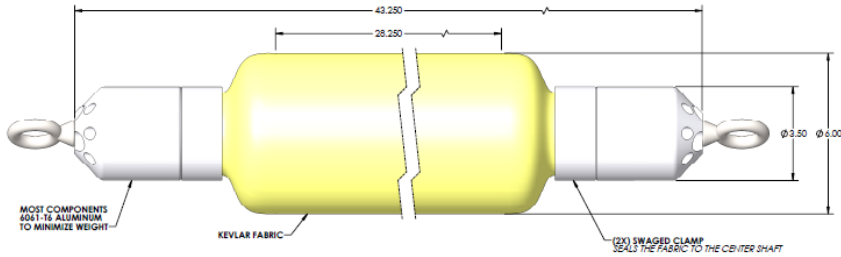
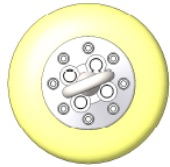
VIALS
CAPS



REV.	DESCRIPTION	DATE	APP.

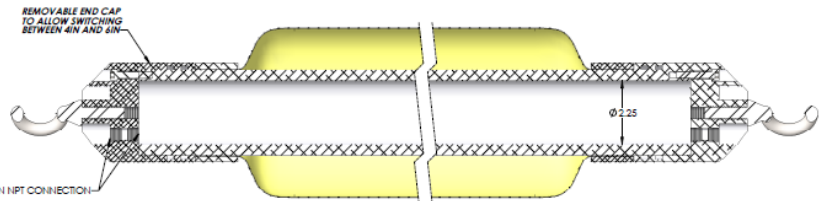
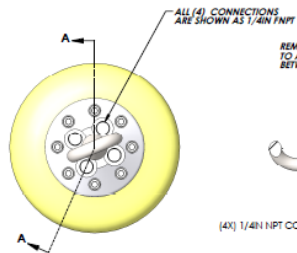


PRELIMINARY

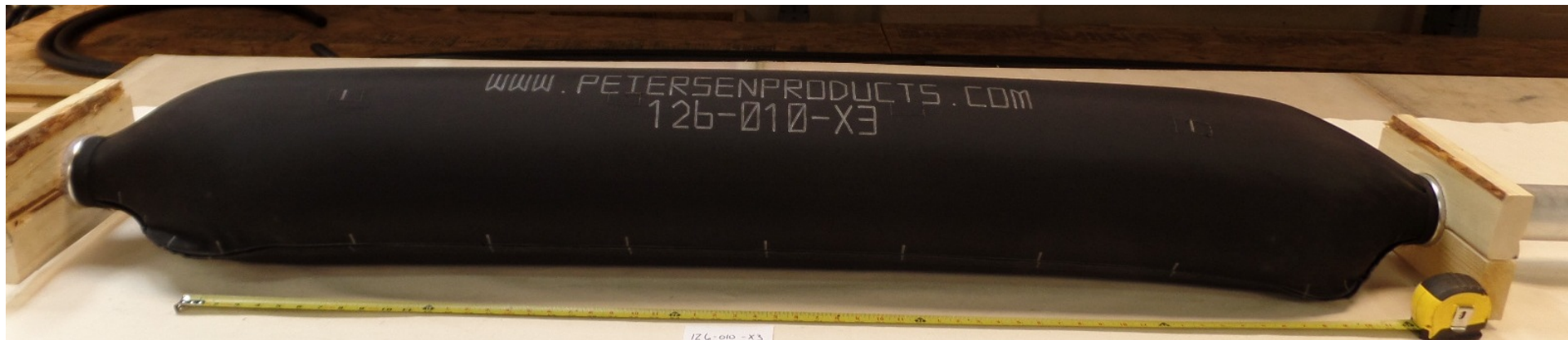
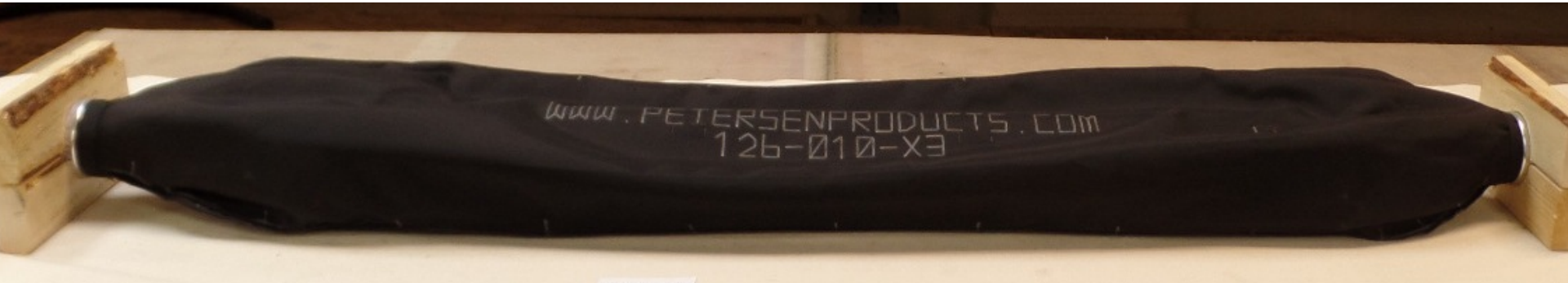


PLUG SPECIFICATIONS:
ESTIMATED UNIT WEIGHT: 25-30LBS
INFLATION PRESSURE: 100 PSI MAX

3D CAD MODEL MODEL NUMBER: 3D-CAD-001 SCALE: 1:1 DATE: 10/1/2018		PETERSEN PRODUCTS CO. LLC MATERIAL: SEE BOM SIZE: REV:	
PREPARED AND CHECKED BY: [REDACTED] DESIGNED BY: [REDACTED] DRAWN BY: [REDACTED] APPROVED BY: [REDACTED]		SEE DWG. NO. C SCALE: 1:2	REV. 0 SHEET 1 OF 2



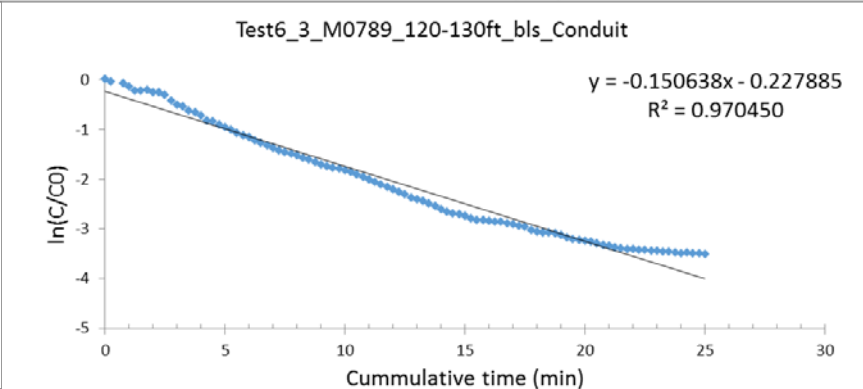
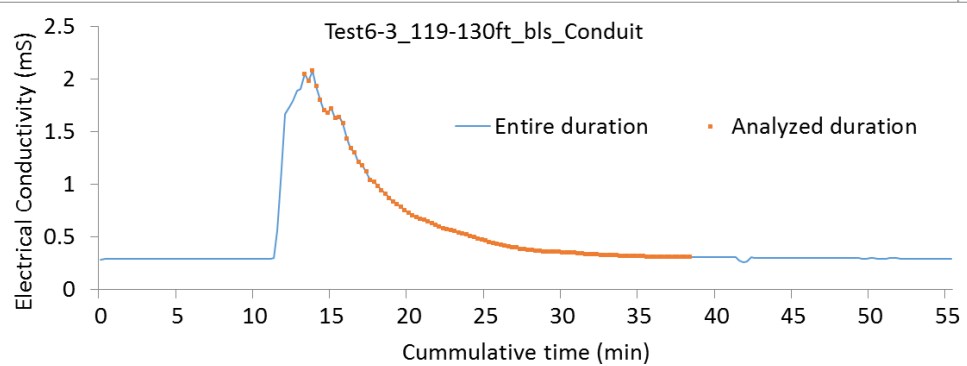
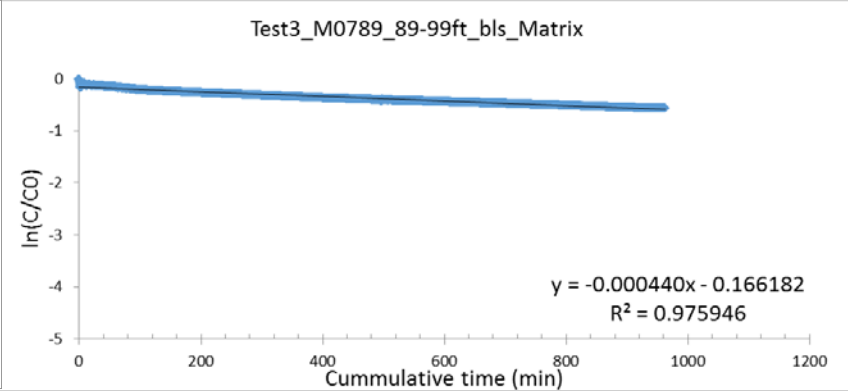
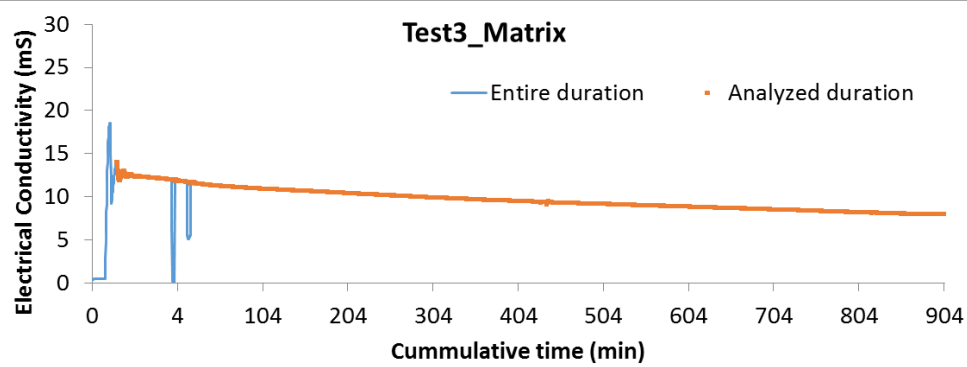
SECTION A-A





matrix vs conduit

variable monitoring periods



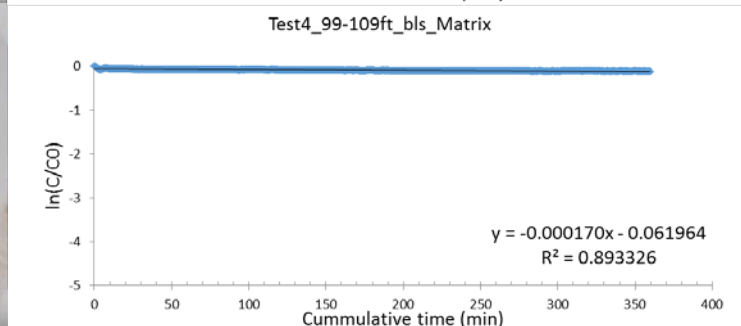
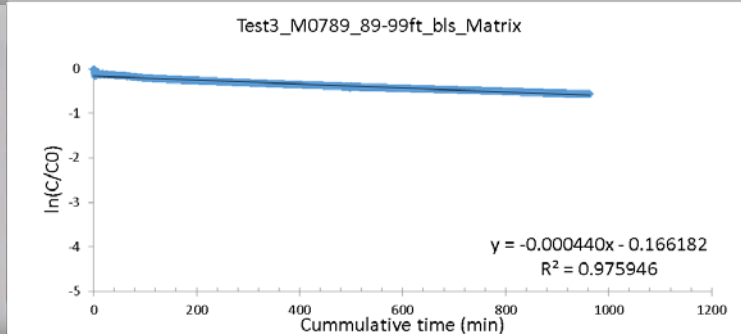
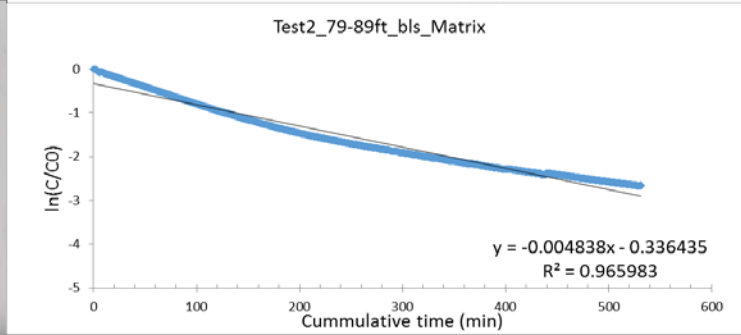
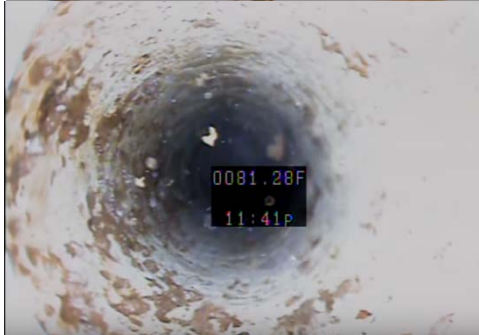
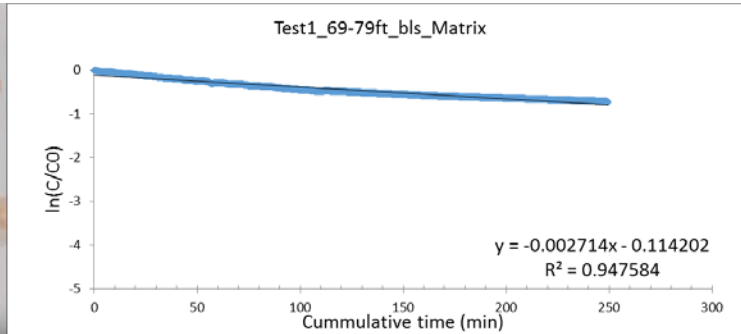
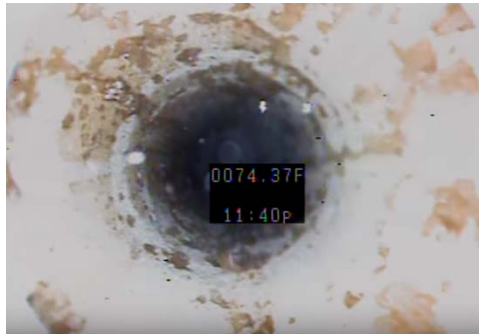
Two tests performed on M0789, at different target depths

- Test 3: 16 hours
- Test 6-3: 25 minutes

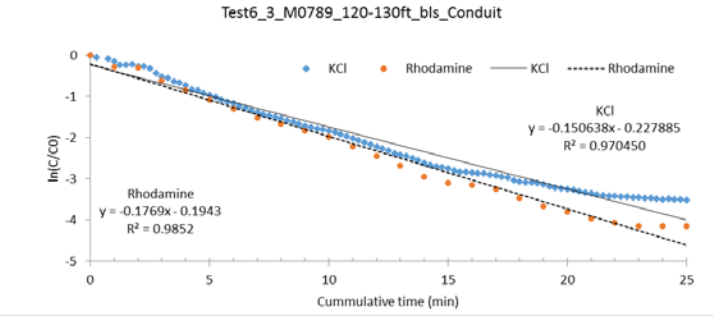
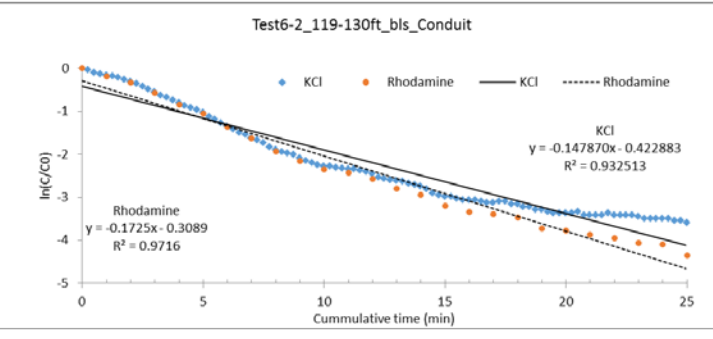
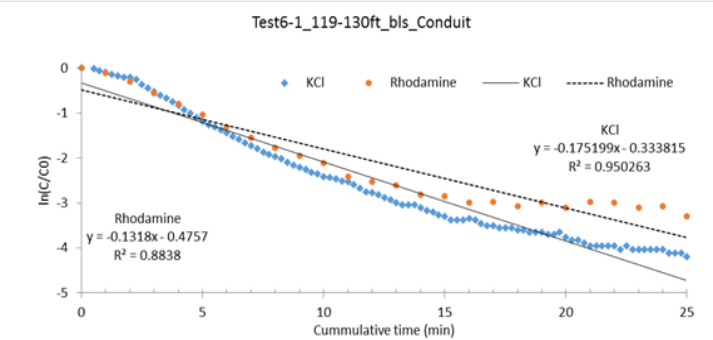
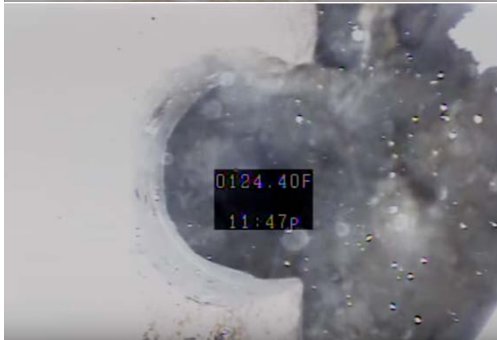
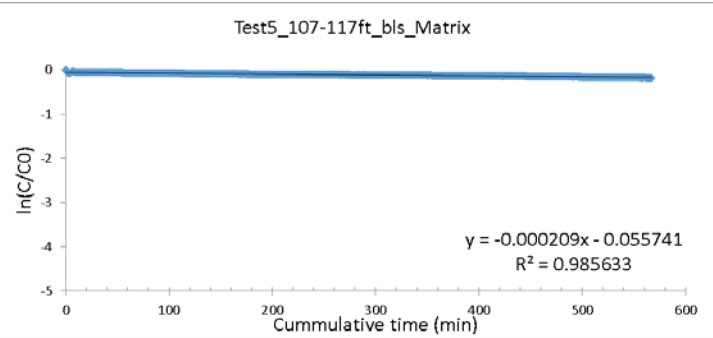
Test 3 never reached background: final conductivity ~8mS

Well M789

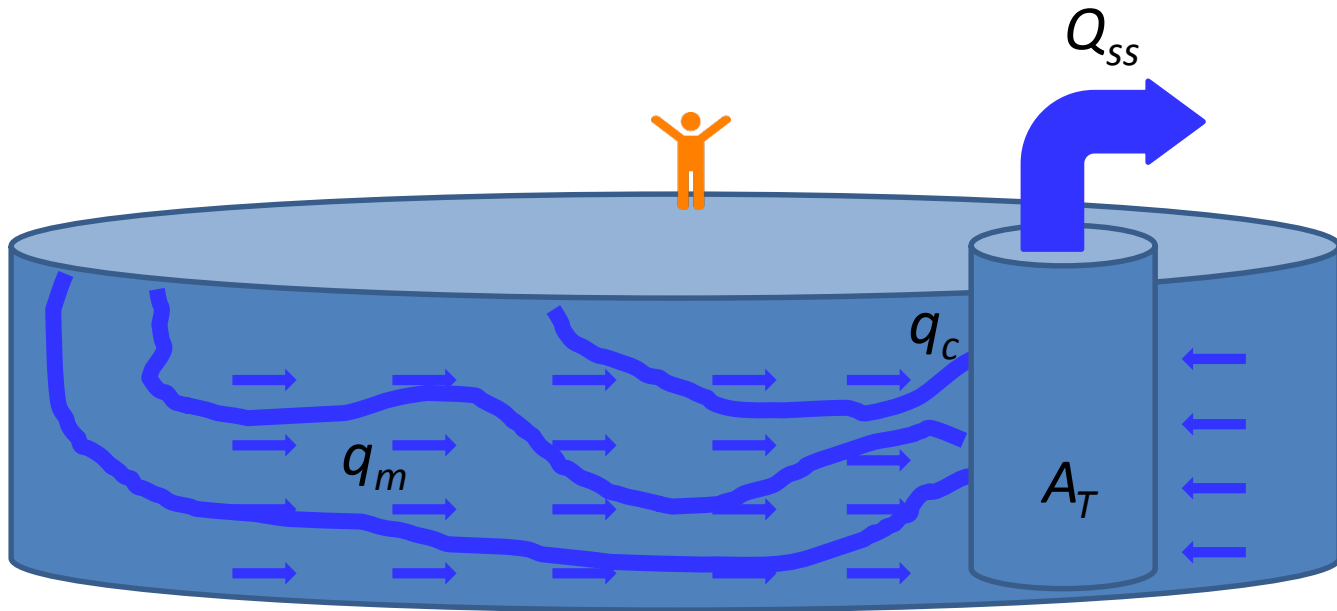
- Video logs vital for identifying potential test depths



Well M789



Test Number	Depth (ft bls)	KCl q(cm/day)	Rhodamine q (cm/day)
1	69-79	16.0	
2	79-89	28.4	
3	89-99	2.6	
4	99-109	1.0	
5	107-117	1.2	
6-1	120-130	1030.2	775.0
6-2	120-130	869.5	1014.3
6-3	120-130	885.8	1040.2



$$Q_{ss} = q_{avg} A_T$$

$$Q_{ss} = Q_m + Q_c$$

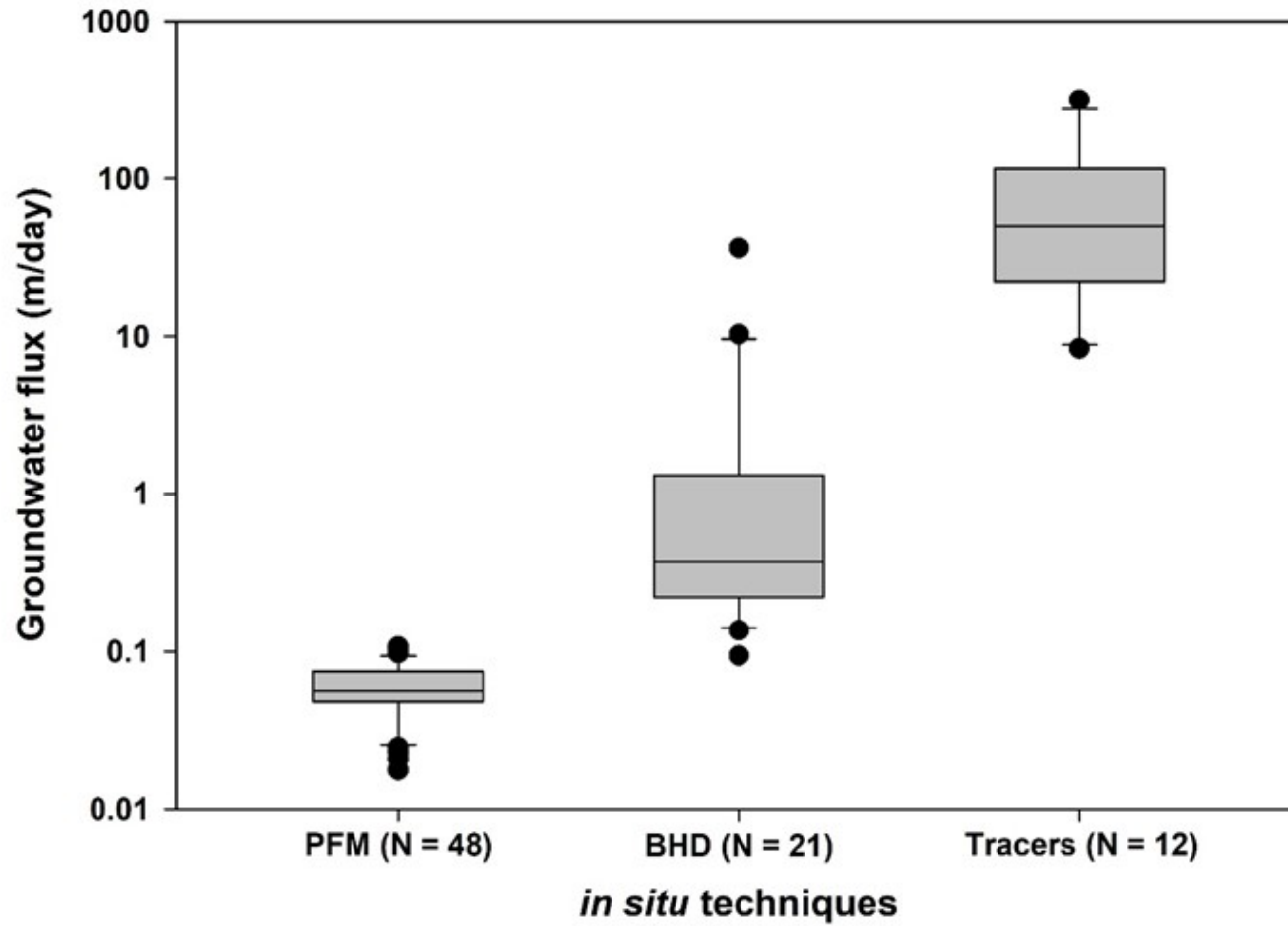
$$Q_{ss} = q_m A_m + q_c A_c$$

$$A_T = A_m + A_c$$

$$\underline{\underline{A_c/A_T = (q_{avg} - q_m)/(q_c - q_m)}}$$

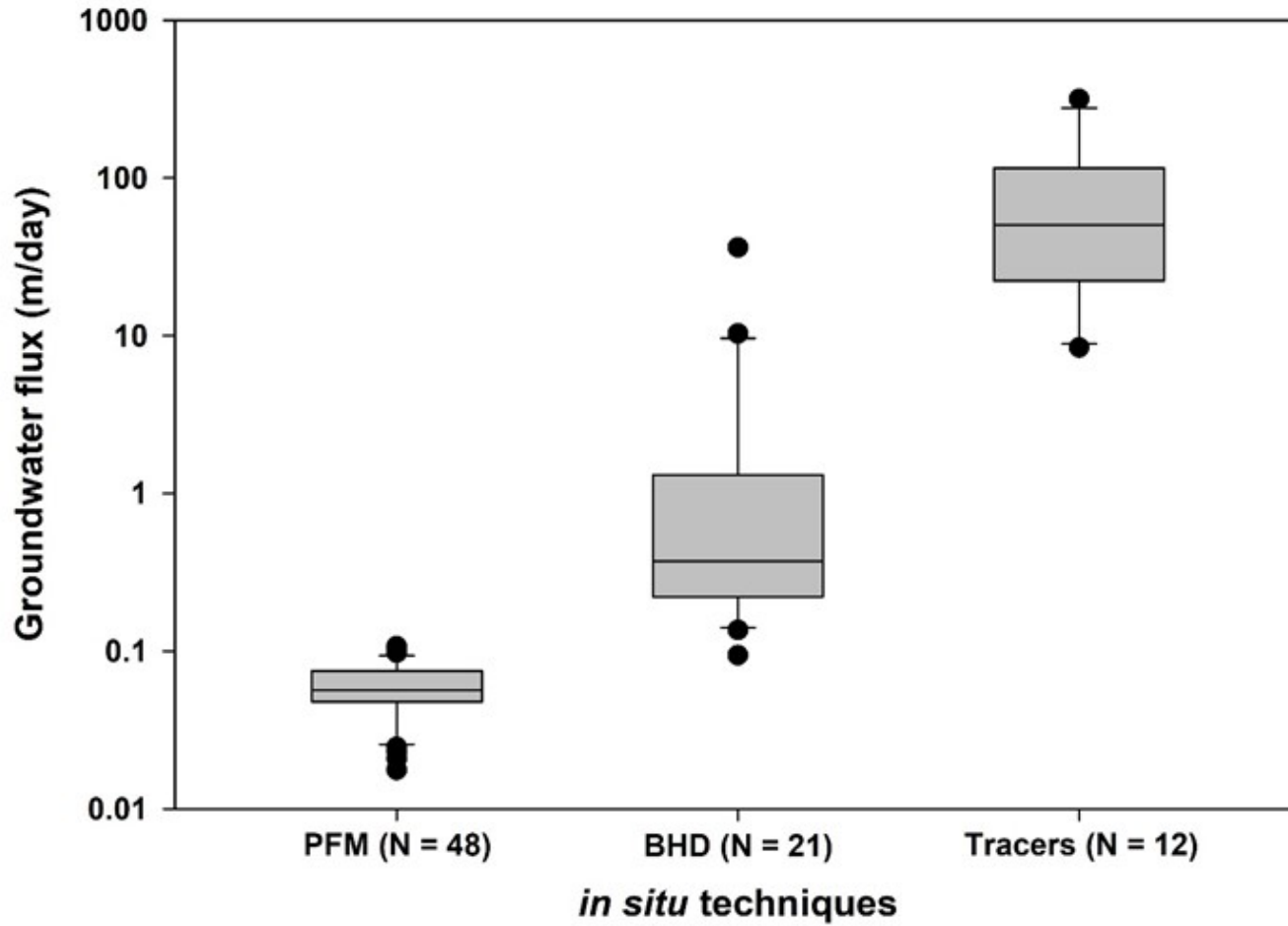
	10-km transect	20-km transect
q_{avg}	1.1 m/d	0.55 m/d
q_m	0.06 m/d	0.06 m/d
q_c	??	??
A_c/A_T		
Q_c/Q_{ss}		

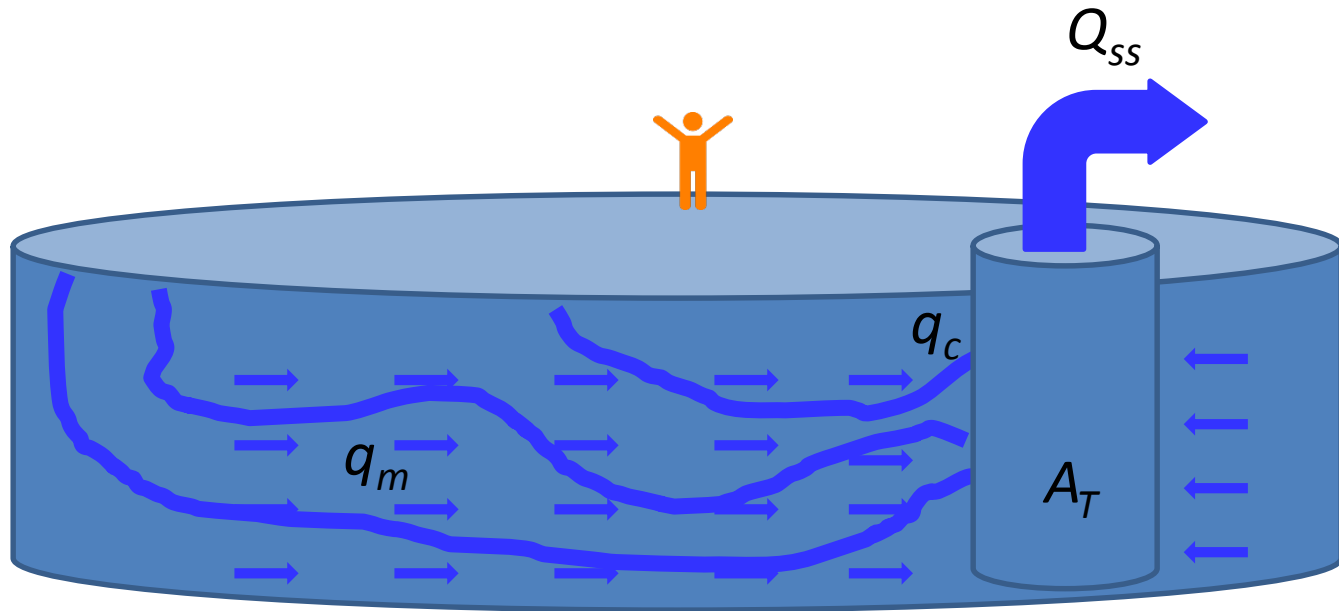
Matrix < 0.1 m/day < Conduit



Matrix < 0.1 m/day < Conduit

	Matrix	Conduit
Average velocity (m/day)	0.06	30.08





$$Q_{ss} = q_{avg} A_T$$

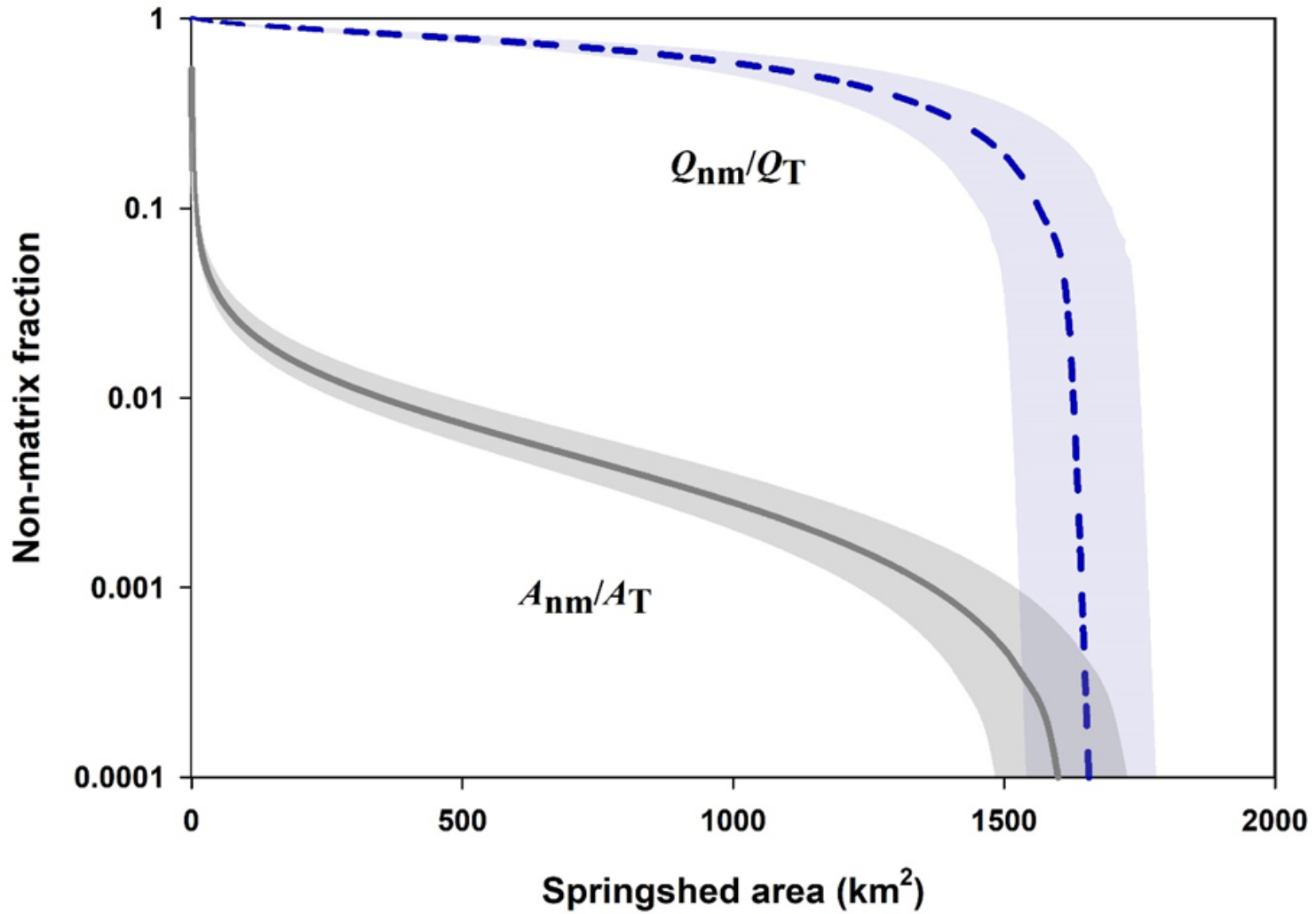
$$Q_{ss} = Q_m + Q_c$$

$$Q_{ss} = q_m A_m + q_c A_c$$

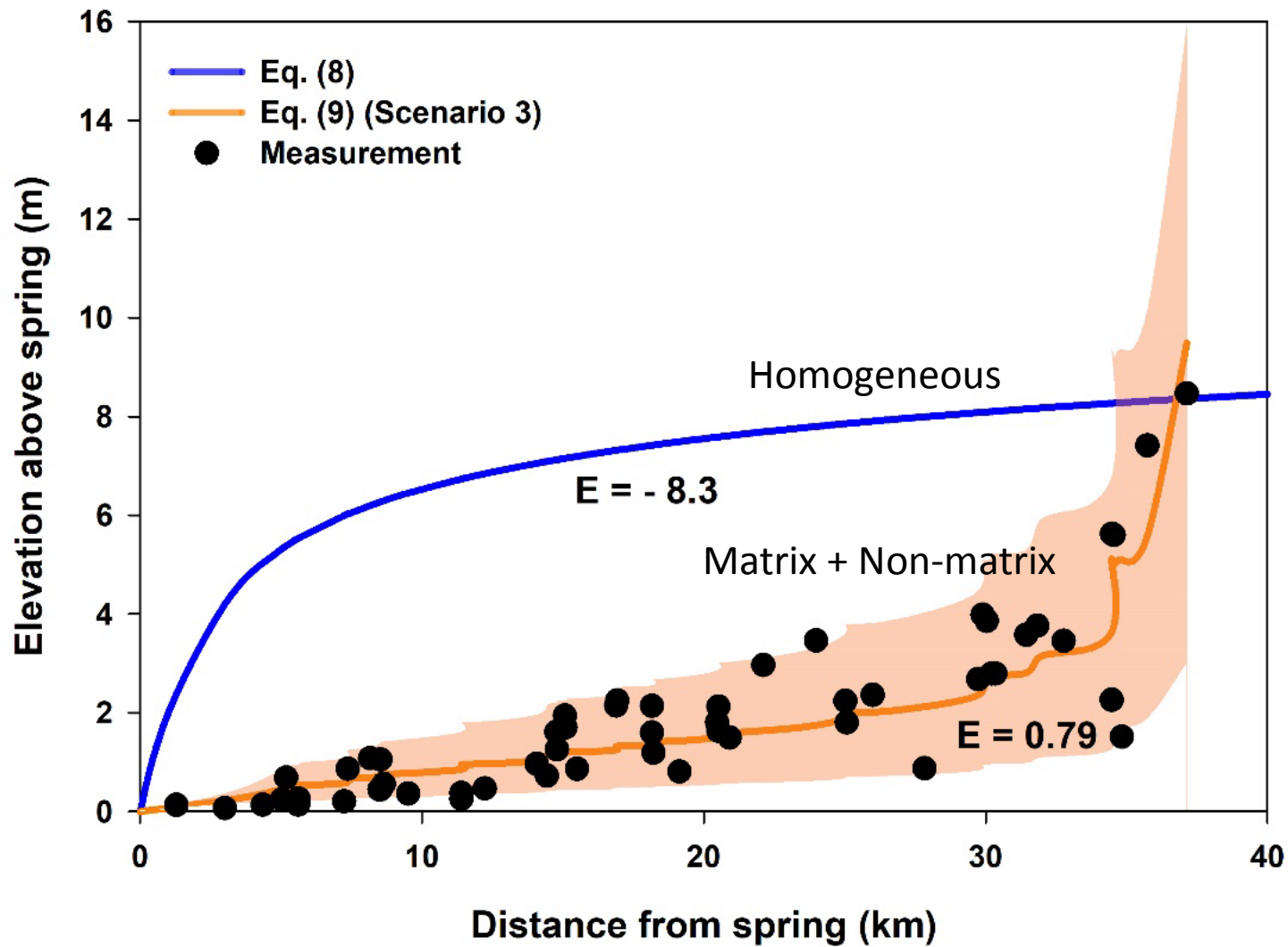
$$A_T = A_m + A_c$$

$$\underline{\underline{A_c/A_T = (q_{avg} - q_m)/(q_c - q_m)}}$$

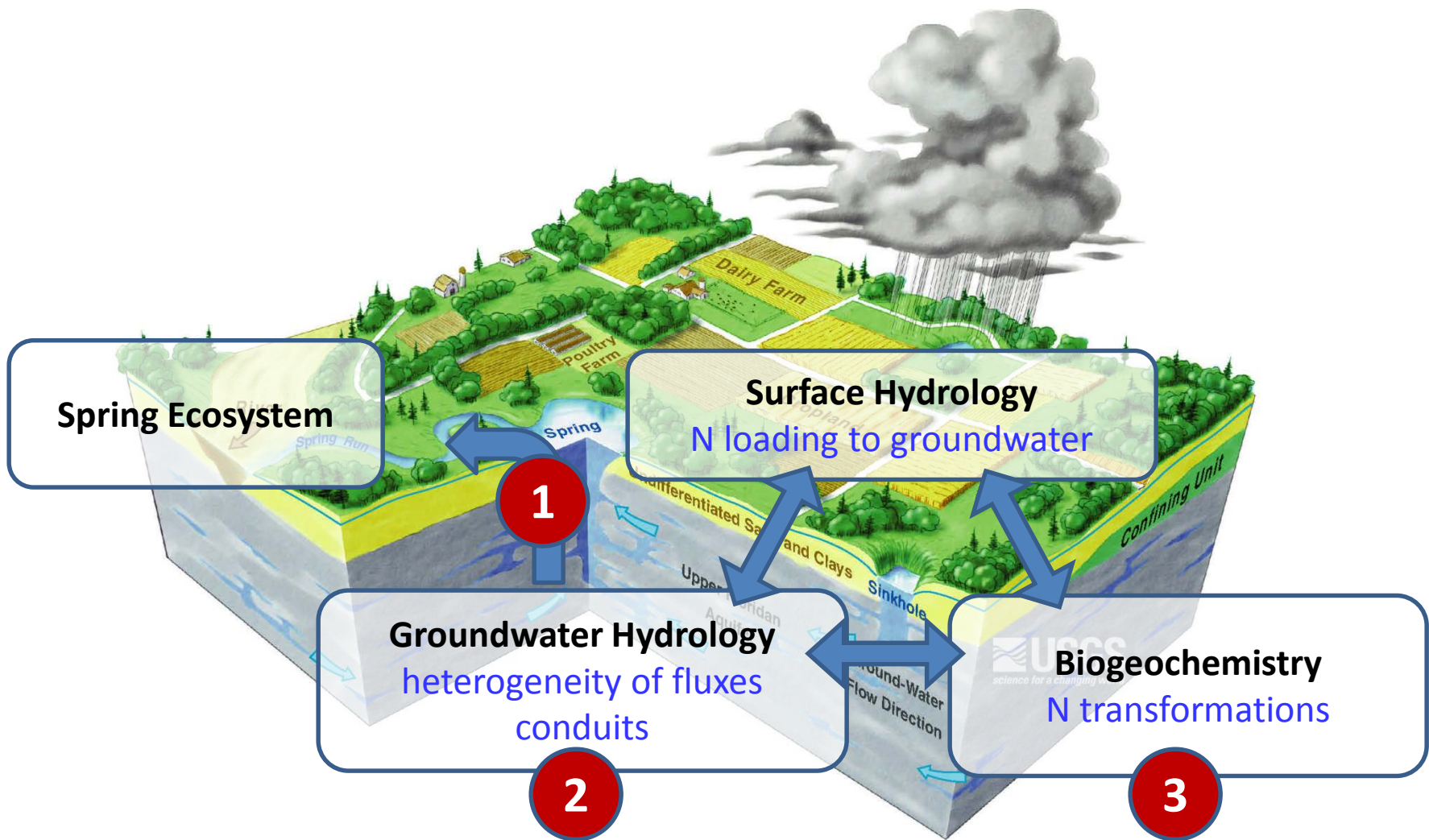
	10-km transect	20-km transect
q_{avg}	1.1 m/d	0.55 m/d
q_m	0.06 m/d	0.06 m/d
q_c	30 m/d	30 m/d
A_c/A_T	0.03	0.016
Q_c/Q_{ss}	0.95	0.89



For $q_m = 0.06$ m/d
 $q_c = 30$ m/d



For $q_m = 0.06$ m/d
 $q_c = 30$ m/d



in conclusion

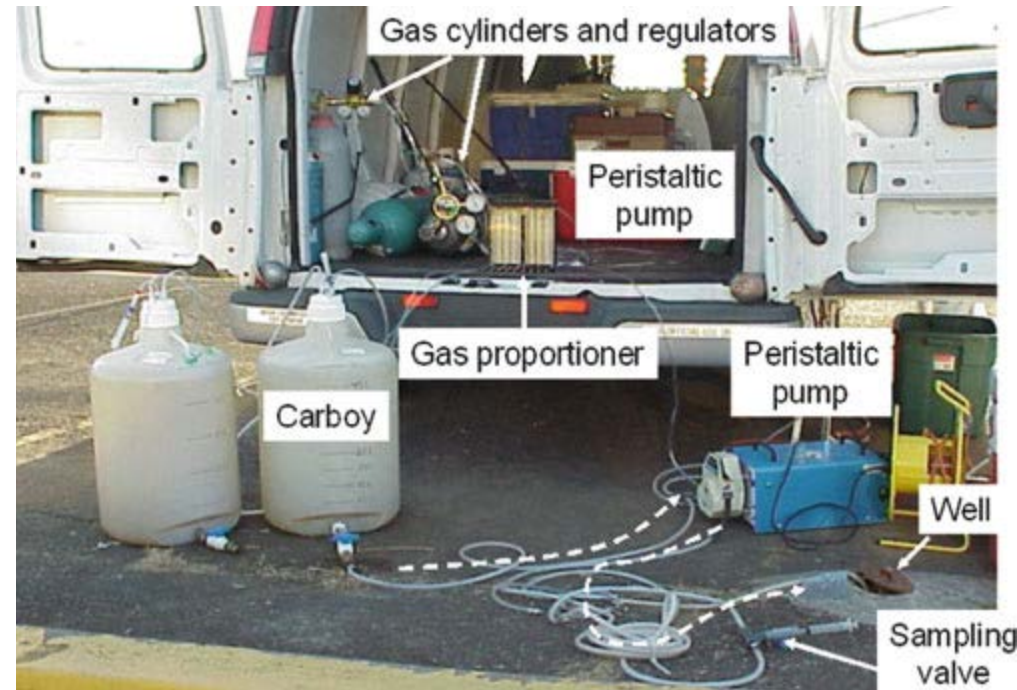
- in situ measurements of groundwater fluxes
 - Passive Flux Meters – mostly rock matrix ~ 0.06 m/d
 - Borehole Dilution Tests – mostly conduits ~ 1 m/d
 - Dye Tracer Tests – only conduits > 10 m/d
- spring flow is almost all from **fast-moving conduits**
 - conduits represent a **tiny fraction** of the aquifer volume
 - groundwater storage is almost all in slow-flowing rock matrix

</end>

Push-Pull Test implementation

Controlled injection of a prepared test solution ("push") into an aquifer followed by the extraction of the test solution ("pull").

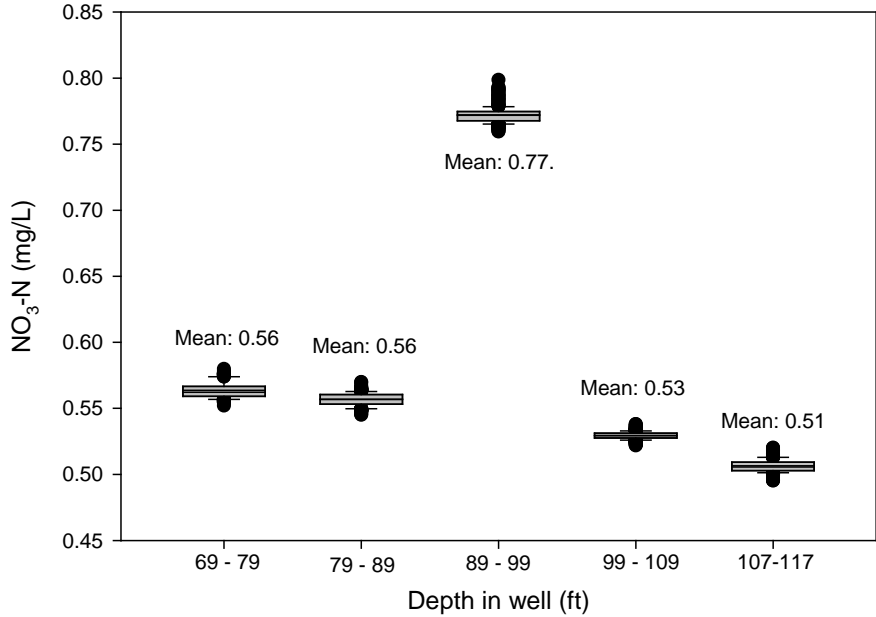
The injected test solution consists of a nonreactive tracer and NO_3^- .



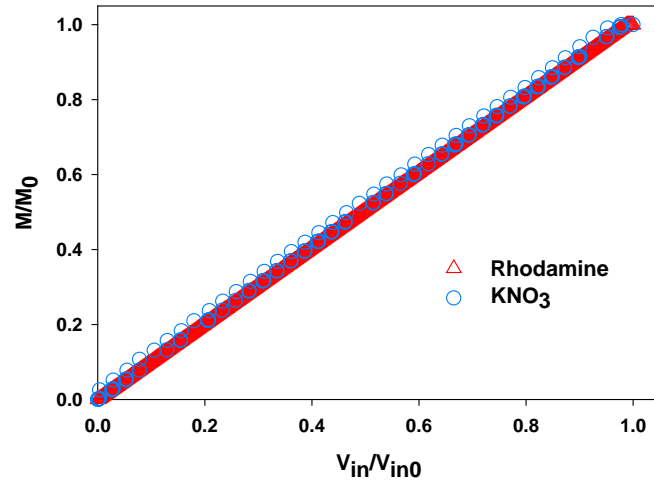
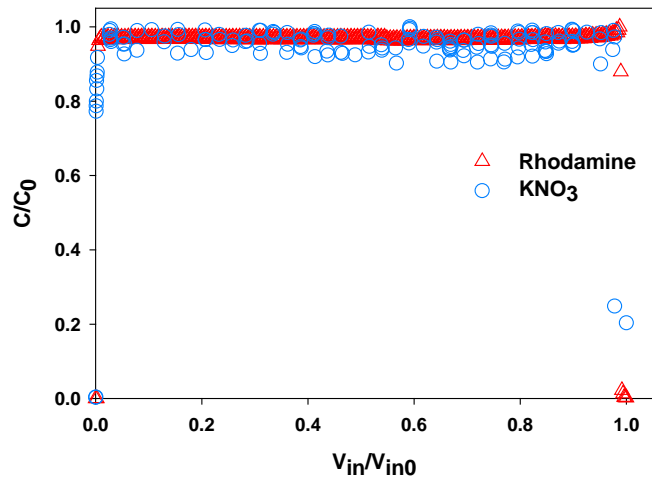
Push-Pull Test at M0789 (89-99ft)



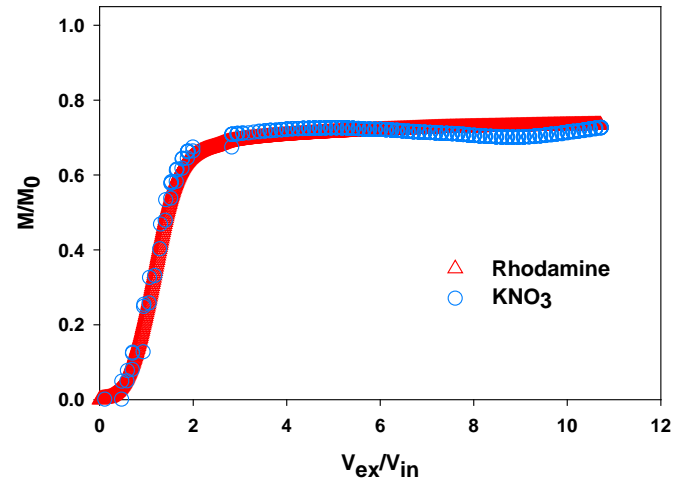
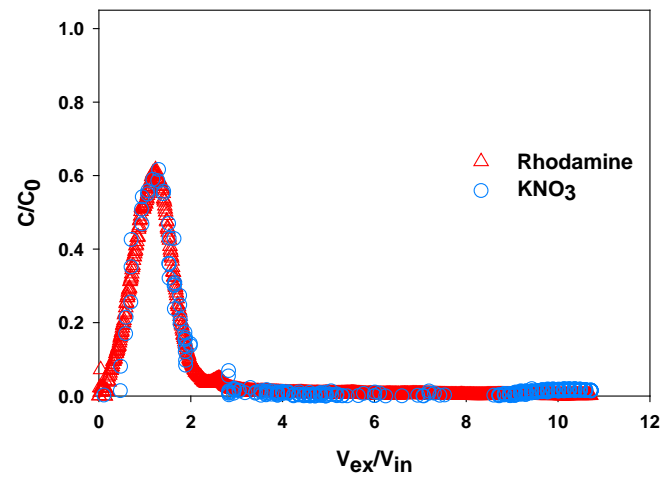
Background Nitrate



M0798 at 89-99ft



PUSH



PULL

Mass Recovery

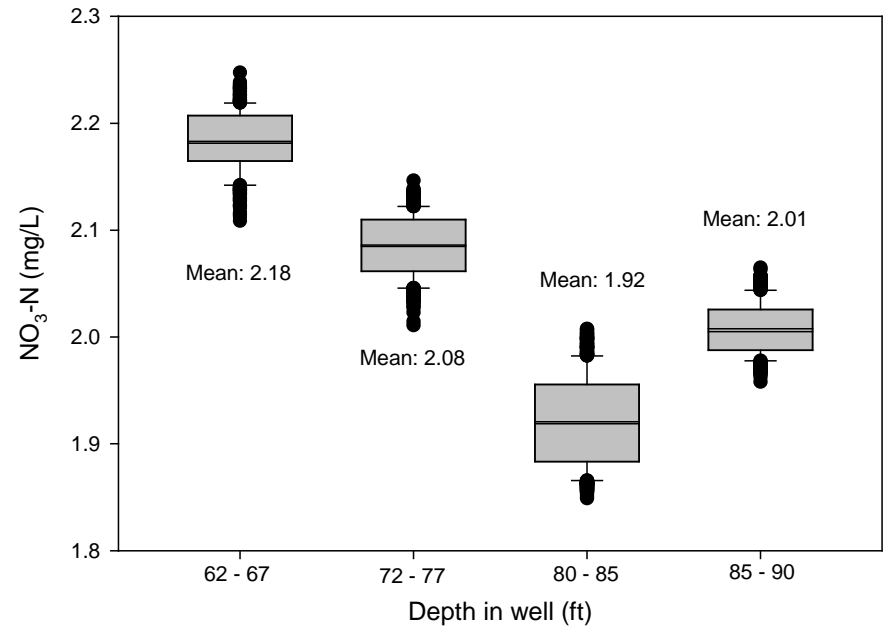
Rhodamine: **73.3%**

KNO_3 : **73.2%**

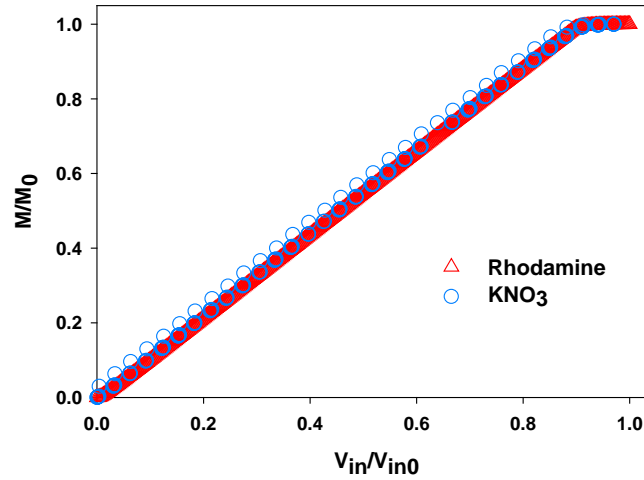
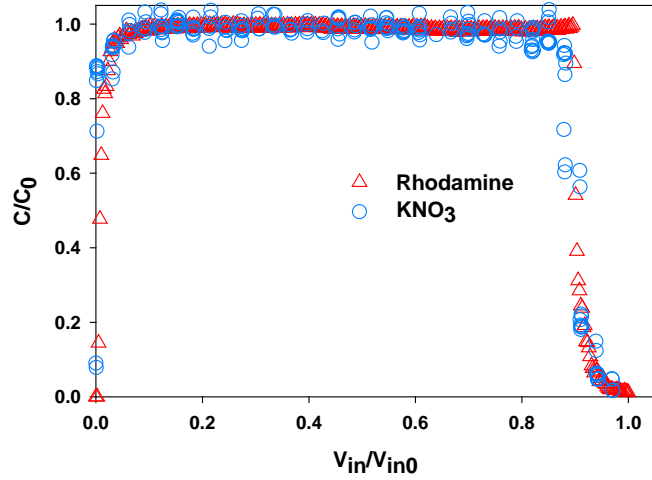
Push-Pull Test at Sprayfield (59-69ft)



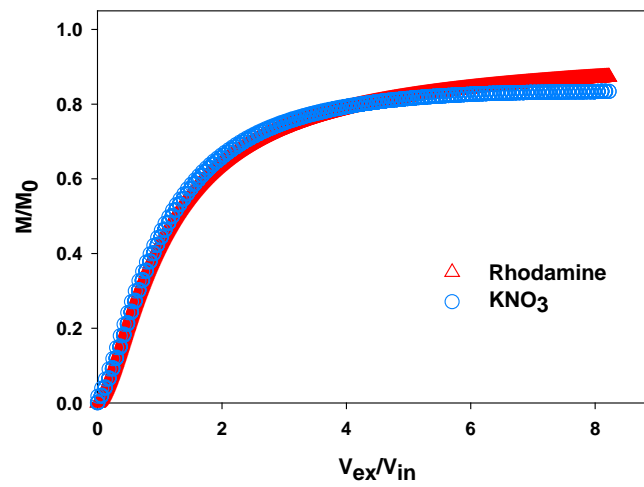
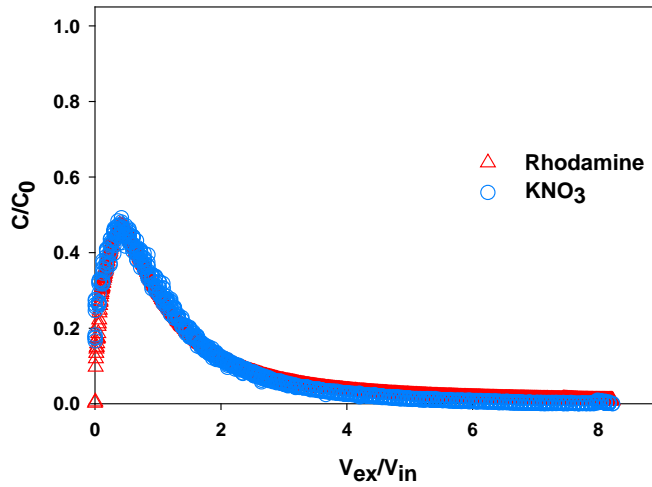
Background Nitrate



Sprayfield at 59-69ft



PUSH



PULL

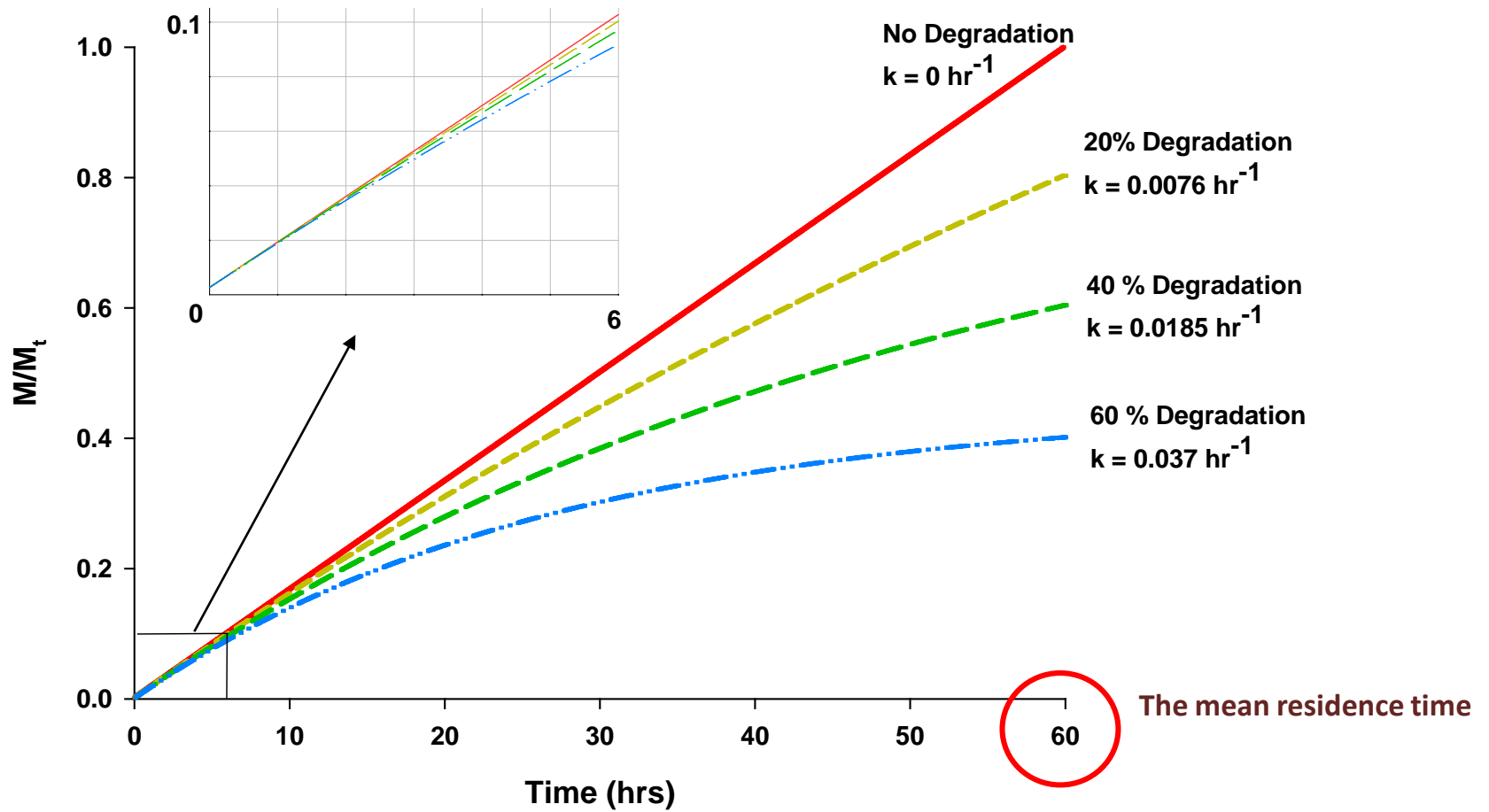
Mass Recovery

Rhodamine: **87.3%**

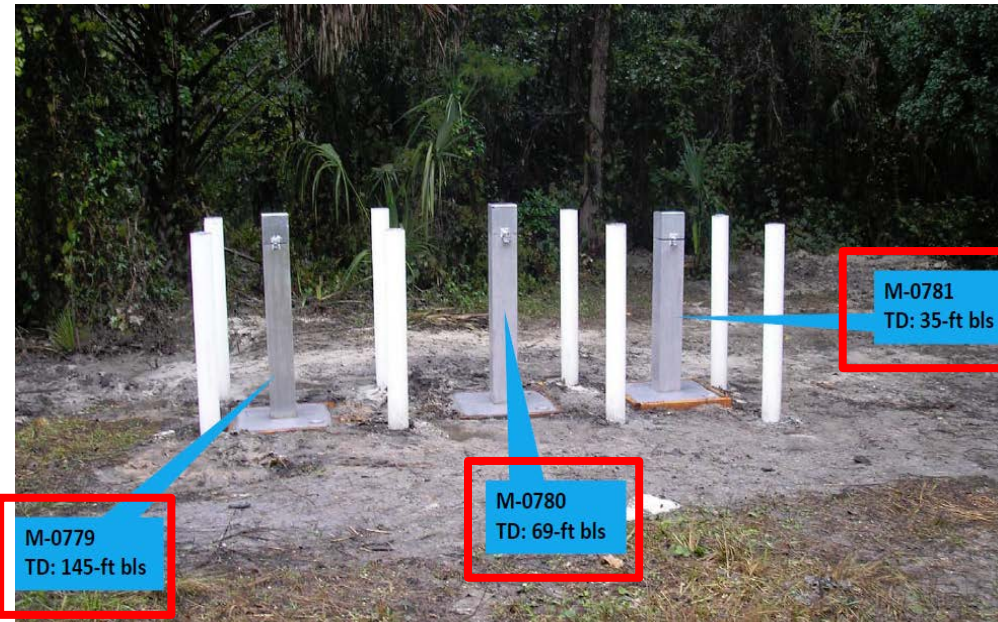
KNO_3 : **83.4%**

No denitrification ???

Estimation of First-order rate constant



Push-Pull Test M779 at 135-145ft



NO nitrate at three wells

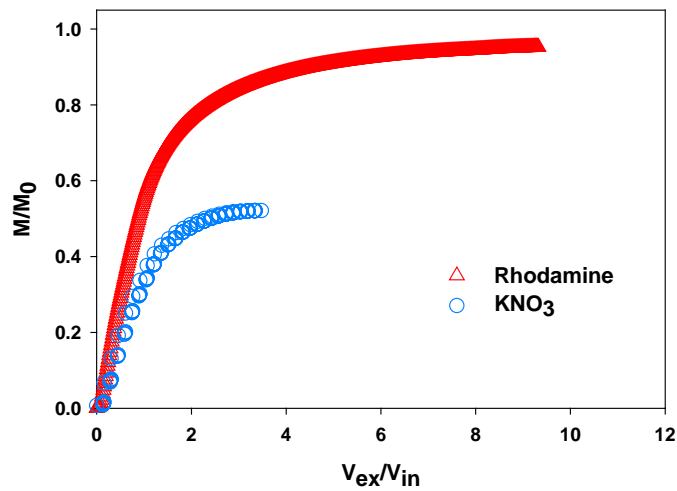
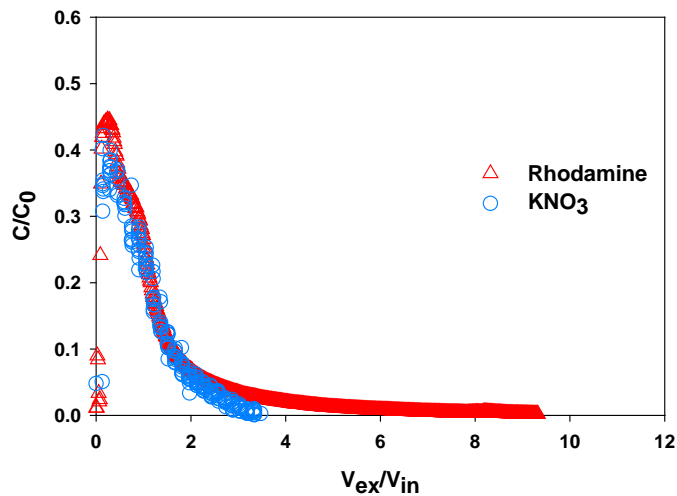
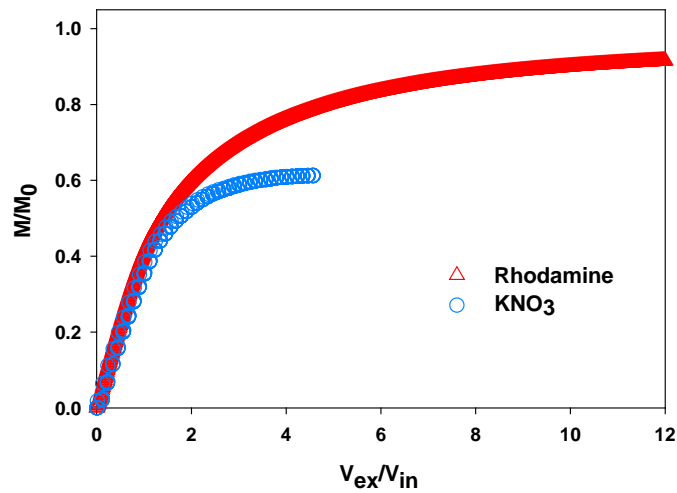
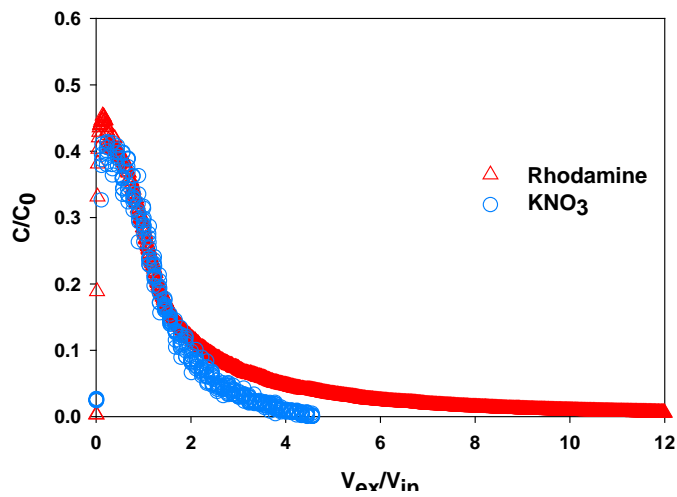


M779 at 135-145ft

Mass Recovery

Rhodamine: **93.9%**

KNO₃: **61.2%**



Mass Recovery

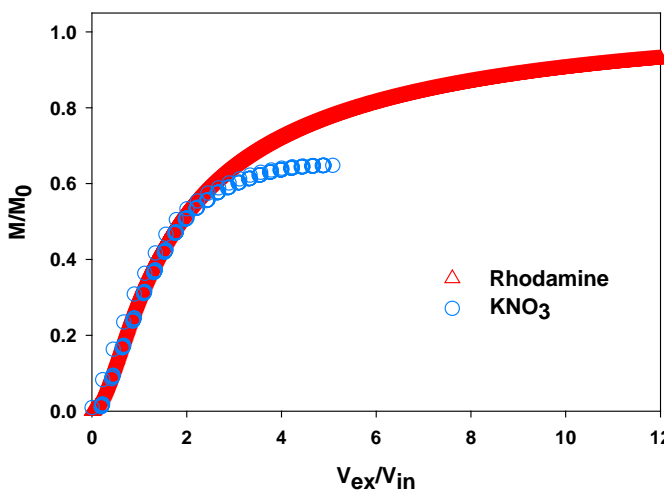
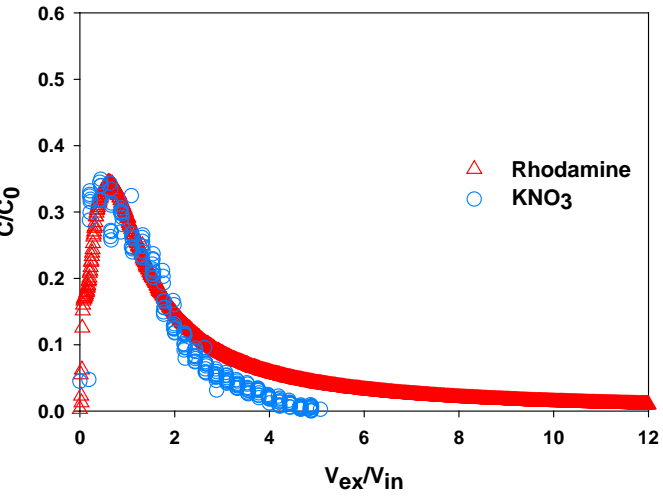
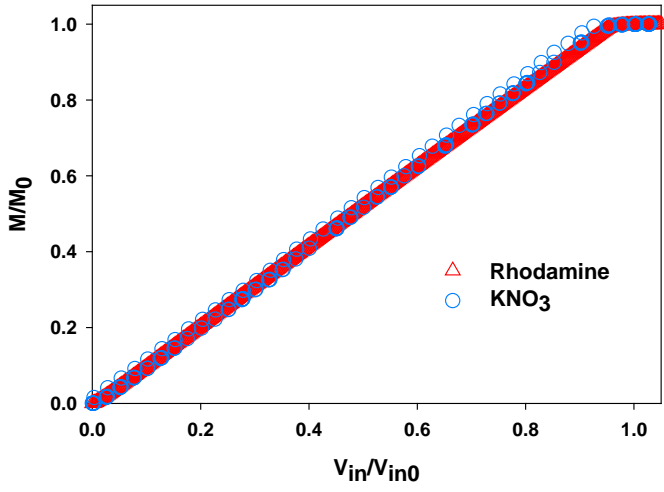
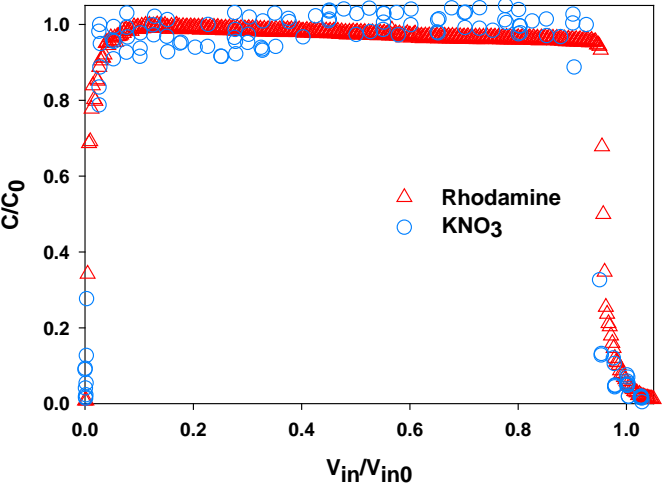
Rhodamine: **95.3%**

KNO₃: **52.1%**

M780 at 59-69ft

Mass Recovery

Rhodamine: **97.1%**
KNO₃: **64.8%**

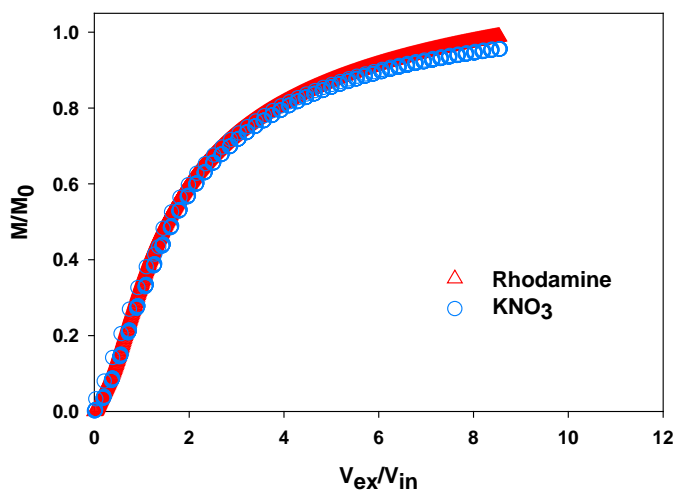
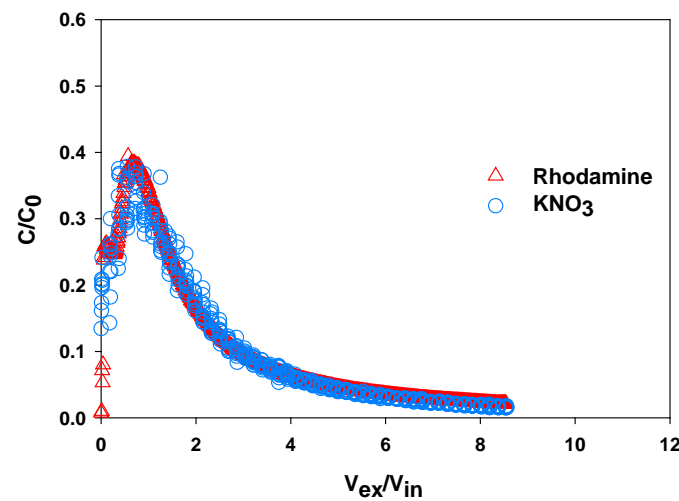
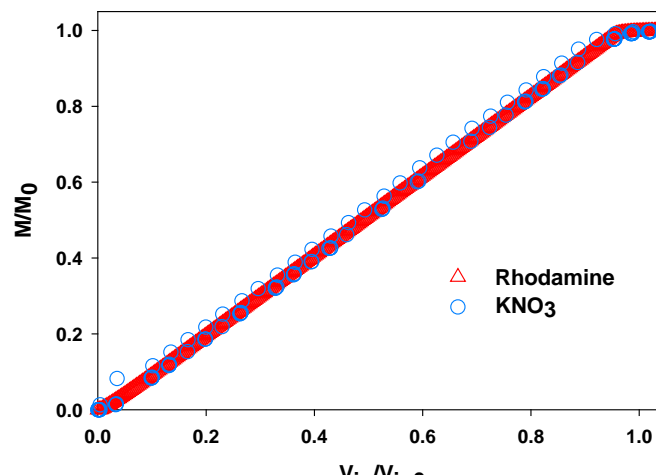
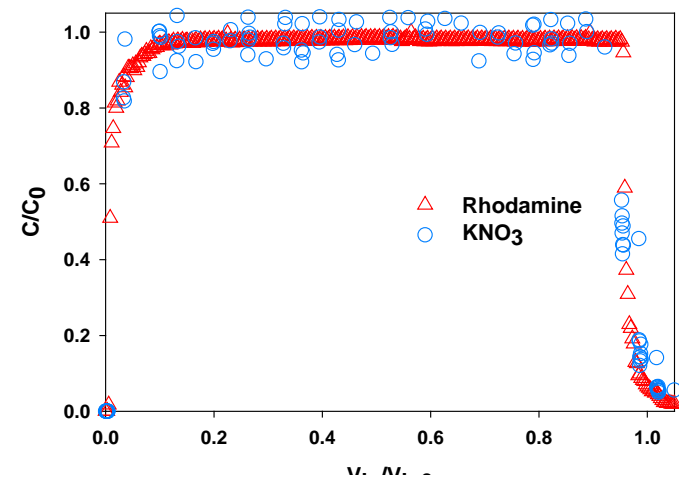


M781 at 25-35 ft

Mass Recovery

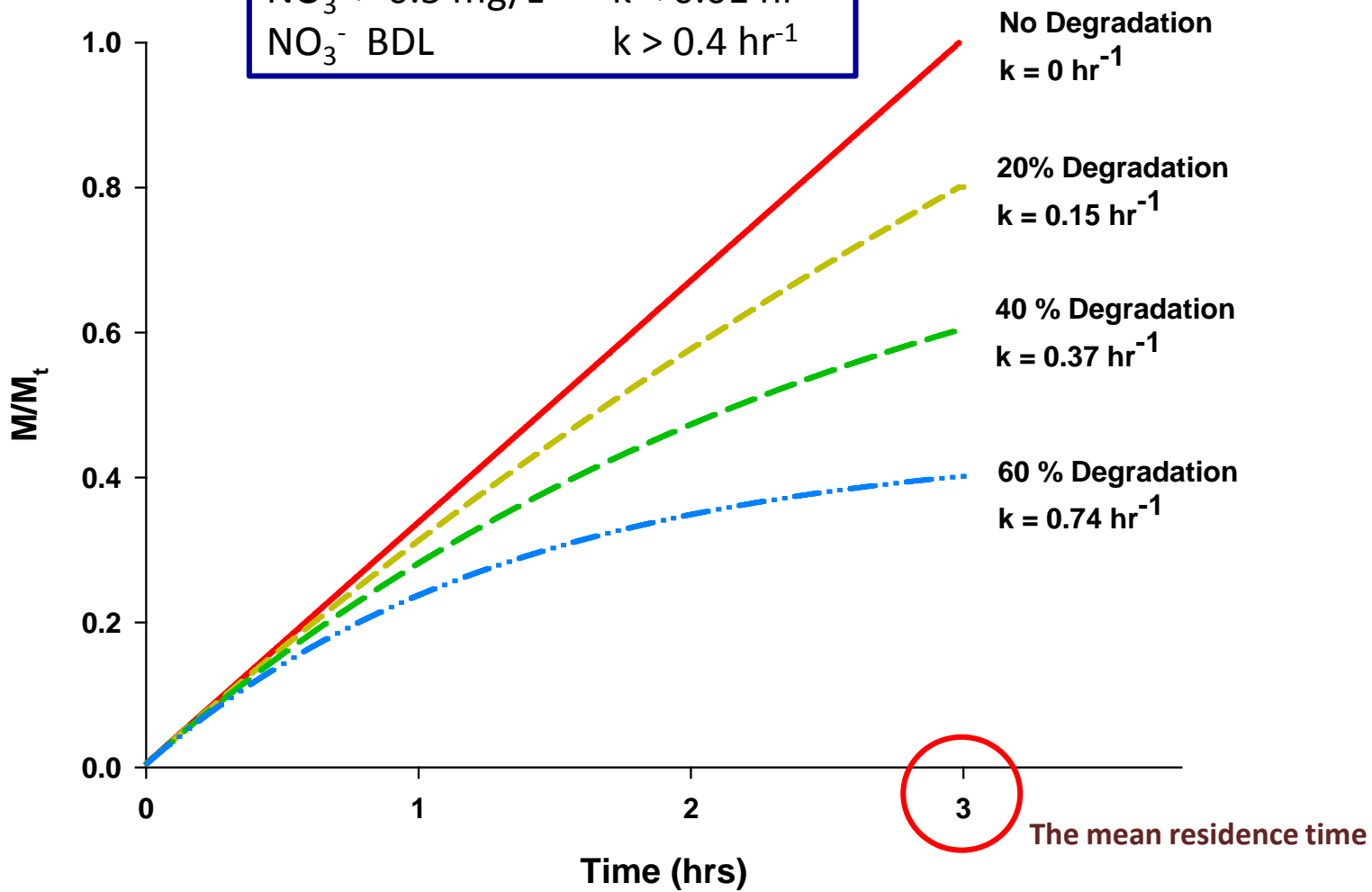
Rhodamine: **98.8%**

KNO₃: **95.6%**



Estimation of First-order rate constant

$\text{NO}_3^- > 0.5 \text{ mg/L}$	$k < 0.01 \text{ hr}^{-1}$
$\text{NO}_3^- \text{ BDL}$	$k > 0.4 \text{ hr}^{-1}$



mostly rainfall with long-time lag (saltwater interface)

